

Air Quality Permitting Statement of Basis

February 8, 2005

Permit to Construct No. P-040101 Interstate Concrete and Asphalt Company, Rathdrum Facility ID No. 055-00048

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FINAL PERMIT

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Acronyms, Units, And Chemical Nomenclatures

AFS AIRS Facility Subsystem

AIRS Aerometric Information Retrieval System

AQCR Air Quality Control Region
CFR Code of Federal Regulations

CO carbon monoxide

DEQ Department of Environmental Quality
EPA U.S. Environmental Protection Agency

gr/dscf grain (1 lb = 7,000 grains) per dry standard cubic foot

HAPs Hazardous Air Pollutants

HMA hot mix asphalt

IDAPA a numbering designation for all administrative rules in Idaho promulgated in accordance with the

Idaho Administrative Procedures Act

lb/hr pound per hour

MACT Maximum Achievable Control Technology

MMBtu/hr million British thermal units per hour
NAAQs National Ambient Air Quality Standard

NESHAP National Emission Standards for Hazardous Air Pollutants

NO_x nitrogen oxides

NSPS New Source Performance Standards

O&M Operation and maintenance

PM particulate matter

PM₁₀ particulate matter with an aerodynamic diameter less than or equal to a nominal 10 micrometers

ppm parts per million

PSD Prevention of Significant Deterioration

PTC permit to construct

RAP Recycled asphalt pavement

RCRA Resource Conservation and Recovery Act
Rules Rules for the Control of Air Pollution in Idaho

SIC Standard Industrial Classification

SIP State Implementation Plan

SO₂ sulfur dioxide
TAP toxic air pollutant
T/hr tons per hour
T/yr tons per year

μg/m³ mierograms per cubic meter

UTM Universal Transverse Mercator

VOC volatile organic compound

1. PURPOSE

The purpose for this statement of basis is to satisfy the requirements of IDAPA 58.01.01.200, Rules for the Control of Air Pollution in Idaho, for issuing permits to construct.

2. FACILITY DESCRIPTION

The Interstate Concrete and Asphalt Company (Interstate) proposes to construct a hot-mix asphalt (HMA) plant at 8849 W. Wyoming Avenue, which is located 0.5 mile west of Highway 41 in Rathdrum. The plant is to be identified as the Wyoming Plant.

In the HMA plant, stockpiled aggregate is transferred to eight cold feed bins. Aggregate is dispensed from the bins onto slow moving feeder conveyors, which transfer the aggregate to the dryer. Recycled asphalt pavement (RAP) material is transferred from stockpiles to a live bottom bin. The bin feeds onto a conveyor to a lump breaker. From the lump breaker, a conveyor feeds the RAP material to the dryer where both aggregate and RAP are heated in the dryer. Aggregate and RAP travel through the rotating drum dryer counter current to the heating media. The material is then heated and dried and mixed with liquid asphalt cement. The resulting HMA is then conveyed to hot storage bins until it can be loaded into dump trucks for transport off site or transferred via a conveyor to silos for temporary storage.

This PTC is for a new CMI HMA plant, rated at 400 T/hr. Particulate matter emissions from the HMA plant are controlled by a baghouse.

3. FACILITY / AREA CLASSIFICATION

Interstate is classified as a synthetic minor facility because enforceable operational limits limit the facility's potential to emit to less than Tier I operating permit major source thresholds. The AIRS facility classification is "SM80" because the facility's potential to emit is within 80% of the Tier I operating permit major source threshold level for a criteria air pollutant. The SIC defining this facility is 2951.

The facility is located within AQCR 62 and UTM zone 11. The facility is located in Kootenai County which is designated as unclassifiable for all criteria pollutants (PM₁₀, CO, NO_X, SO₂, lead, and ozone).

The AIRS information provided in Appendix B lists the classification for each regulated air pollutant at this facility. This required information is entered into the EPA AIRS database.

4. APPLICATION SCOPE

Interstate submitted a PTC application for the construction of a new HMA plant with the following parameters:

- The maximum hourly production rate of the HMA plant is 400 T/hr.
- The HMA plant will be configured with recycled asphalt pavement (RAP) equipment.
- The annual production rate of the HMA plant is limited to 1,480,000 tons per any consecutive 12month period (T/yr)
- The annual hours of operation of the HMA plant is limited to 3,700 hours per any consecutive 12-month period (hr/yr).
- Natural gas, liquefied petroleum gas (propane), No. 2 diesel fuel oil, and used oil are the fuel types allowed to be burned in drum dryer.

4.1 Application Chronology

January 26, 2004 DEQ received an application from Interstate for a permit to construct.

The permit number assigned for this project was PTC No. P-040101.

February 24, 2004 DEQ

DEO determined the P-040101 application complete.

March 5, 2004

Interstate requested to review a draft of PTC No. P-040101 prior to the

final issuance.

March 8, 2004

Interstate submitted additional information to DEQ.

March 22 and March 26, 2004

Interstate submitted additional modeling information to DEQ.

April 21, 2004

DEO sent Interstate a copy of draft PTC No. P-040101 for review.

April 29, 2004

DEQ received an email from Interstate in which the company requested to extend issuance of the final PTC until July of 2004. The reason for this is that the new HMA plant is currently in Montana and will not be

back to Rathdrum facility until July or August of 2004.

June 1, 2004

A public comment period started on June 1, 2004, and ended on June 30, 2004. Comments were received from a citizen. The comments and DEQ's response to the comments are included in Appendix E of this

statement of basis.

5. PERMIT ANALYSIS

This section of the statement of basis describes the regulatory requirements for this PTC action.

5.1 Equipment Listing

Hot-mix Asphalt Plant

Manufacturer: CMI PTD-400
Type of HMA plant: Drum mix

Maximum hot-mix asphalt production rate: 400 T/hr

HMA burner fuel type: Natural gas, propane, ASTM Grade 2 fuel oil, and used oil

Baghouse

Manufacturer: CMI Model: RA3-18P

Drum dryer maximum rated heat input capacity: 120 MMBtu/hr

This permit adds equipment associated with the use of RAP in the HMA plant process, including an additional four bins, a lump breaker, and two conveyors.

Maximum rated heat input capacity: 120 million British thermal units per hour (MMBtu/hr)

5.2 Emissions Inventory

Emissions estimates were provided by Aspen Consulting and Engineering (Aspen) and are included in the PTC application materials submitted to DEQ on January 26, 2004. Appendix A of this statement of basis contains the emissions estimates for particulate matter (PM), particulate matter with an aerodynamic diameter less than or equal to a nominal 10 micrometers (PM₁₀), carbon monoxide (CO), sulfur dioxide (SO₂), volatile organic compounds (VOC), and oxides of nitrogen (NO_x) that were provided by the facility and are shown in Table 5.2.1. Toxic air pollutants (TAPs), and hazardous air pollutants (HAPs) emissions estimates that were provided by the facility are shown in Appendix A of

this document. Emissions estimates of PM, PM₁₀, CO, SO₂, VOC, NO_x, TAPs, and HAPs from the HMA plant dryer at the facility were obtained from emission factors described in U.S. EPA's Compilation of Air Pollutant Emission Factors, AP-42, Section 11.1, Hot Mix Asphalt Plant, 12/00. The hourly emission rates were estimated using the maximum HMA production rate of 400 T/hr. The annual emissions rates were determined based on HMA production limit of 1,480,000 T/yr and operations of 3,700 hours per any consecutive 12-month period.

Table 5.2.1 POTENTIAL EMISSIONSA FROM THE HMA PLANT DRYER

Source Description	Pi	M,	PM	[10 ^c	C	O*	NO	'x *	so) ₂ [†]	VC)Ct	P	p,
[lb/hr	T/yr	Lb/hr	T/yr	lb/hr	T/yr	lb/hr	T/yr	lb/hr	T/yr	lb/hr	T/yr	lb/br	T/yr
HMA drum mix dryer stack	13.2	24.42	9.20	17.02	52.00	96 .20	22.00	40.7	23.20	42.92	12.8	23.68	0.006	0.011

- Emissions were determined by using emissions factors from AP-42, Section 11.1, Hot Mix Asphalt Plants and process limits (e.g. throughput and
- hours of operation)

 Particulate matter
- Particulate matter with an aerodynamic diameter less than or equal to a nominal 10 micrometers
- d Carbon monoxide
- * Nitrogen oxides
- Sulfur dioxide
- Volatile organic compound
- Lead

It should be noted that Interstate will use cold aggregate and RAP in the HMA process. Although the percentage of RAP use will vary, Interstate plans an equal swap of RAP for cold aggregate. As a result, no PM emissions increase will occur as explained below.

RAP emissions are discussed in two sections in AP-42, Section 11.1 for Hot Mix Asphalt Plants. Section 11.1.1.3, Counterflow Drum Mix Plants, states, "...A counterflow drum mix plant can normally process RAP at ratios up to 50 percent with little or no observed effect upon emissions." Section 11.1.2.2, Parallel Flow Drum Mix Plants, states, "...Although it has been suggested that the processing of RAP materials at these type plants may increase organic compound emissions because of an increase in mixing zone temperature during processing, the data supporting this hypothesis is very weak. Specifically, although the data show a relationship only between RAP content and condensible organic particulate emissions, 89 percent of the variations in the data were the result of other unknown process variables." Additionally, none of the emission factor tables in Section 11.1, AP-42 differentiates between aggregate types and RAP. The emission estimates for this permitting action are based on AP-42 emission factors. The calculations do not show an increase in emissions from the using of RAP in the process line.

Also, the use of used oil in the dryer will not result in increase of PM or PM₁₀ emissions, as indicated in AP-42, Table 11.1-3 footnote (g), pertaining to the particulate matter emissions, as follows; "drum mix dryer fired with natural gas, propane, fuel oil, used oil, and coal. The data indicate that fuel type does not significantly effect PM emissions." Therefore, the PM and PM₁₀ emissions estimates for the facility are not expected to increase as a result of the additional types of fuel.

From AP-42, for all other pollutants, the emission factors for each type of fuel were compared, and the highest value for each pollutant was used to calculate the estimated emissions.

The TAPs and HAPs emissions in the permit application were also based on processing of HMA of 1,480,000 T/yr and on operations of 3,700 hours per any consecutive 12-month period. Potential emissions of any single HAP were estimated to be less than 10 T/yr. Potential emissions for two HAPs or more were estimated to be 7.1 T/yr, which are well below the major source threshold of 25 T/yr for a combination of two HAPs or more – refer to Appendix A.

These emissions calculations provided the basis for the emissions limits for CO from the HMA plant dryer stack. They also provided the basis for CO, SO₂, and NO_x, compliance with the National Ambient Air Quality Standards (NAAQS) and the TAPs increment analyses – see Appendix B of this document for modeling analysis.

Detailed emissions estimates are included in Appendix A of this statement of basis. It should be noted that the point source information contained in this table was used to determine the processing fee assessed in accordance with IDAPA 58.01.01.225.

5.3 Modeling

Refer to the modeling review memorandum contained in Appendix C of this statement of basis for a discussion of the air dispersion analysis conducted for this project. Based on the modeling review memorandum, DEQ has determined that emissions of CO, SO₂, and NO₂ from the facility have been successfully demonstrated to not cause or significantly contribute to violations of NAAQs. The PM₁₀ emissions were not modeled, because the net PM₁₀ emissions decreased as a result of replacing the dryer at the facility. Section 2.0 of DEQ's Air Quality Modeling Guideline states: "A modeling analysis is generally required with each permit application for new construction or a modification that results in an increase in emissions of pollutants for sources permitted by DEQ."

The modeling results for the CO, SO₂, and NO₂ are summarized in Table 5.3.1.

Pollutant	Averaging Period	Facility Ambient Impact (µg/m³)*	Background Concentration (µg/m³)*	Total Ambient concentration (µg/m³)²	NAAQS³ (μg/m³)²	Percent of NAAQS ^b
СО	l-hour	349.4	3,600	3,949.4	40,000	9.9
	8-hour	105.0	2,300	2,405.0	10,000	24
SO ₂	3-hour	75.4	34	109.4	1,300	8.4
	24-hour	18.6	26	44.6	365	12.2
	Annual	0.75	8	8.75	80	10.9
NO ₂	Annual	0.72	17	17.72	100	17.7

Table 5.3.1 CO, SO₂, AND NO₂ AMBIENT IMPACT ANALYSIS RESULTS

The TAPs emissions that exceeded the screening emission limits of IDAPA 58.01.01.585-586 are modeled and are included in Appendix C of this statement of basis. A summary of the modeled TAPs are included in Table 5.3.2 below. All TAPs emissions from this facility show compliance with the TAPs increments in accordance with IDAPA 58.01.01.585-586.

Table 5.3.2 TOXIC AIR POLLUTANT AMBIENT IMPACT RESULTS							
Pollutant	Modeled Concentration (µg/m³)*	Toxic Air Pollutant Standard (µg/m³)*	Percent of Toxic Air Pollutant Standard				
2,3,7,8-TCDD	4.0E-11	2.2E-8	0.18				
Acetaldehyde	1.7E-2	0.45	3.8				
Arsenic	6.5E-6	2.3E-4	2.8				
Benzene	5.1E-3	0.12	4.3				
Benzo(a)pyrene	6.5E-6	3.0E-4	2.2				
Cadmium	6.5E-6	5.6E-4	1.2				
Chromium	1.98E-3	25	0.008				
Formaldehyde	4.0E-2	0.077	51.9				
HCI	0.076	375	0.02				
Chromium VI	6.5E-6	8.3E-5	7.8				
Nickel	8.2E-4	4.2E-3	19.5				
Phosphorus	0.01	5	0.2				
Propionaldehyde	0.047	21.5	0.21				
Quinone	0.057	20	0.29				

Micrograms per cubic meter

Micrograms per cubic meter

National Ambient Air Quality Standards

5.4 Regulatory Review

This PTC is subject to the following permitting requirements:

IDAPA 58.01.01.201...... Permit to Construct Required

Interstate proposes to construction a stationary source that does not qualify for a PTC exemption in any of Sections 220 through 223 of the Rules. Therefore, a PTC is required.

IDAPA 58.01.01.203...... Permit Requirements for New and Modified Stationary Sources

All PTC applications are required to demonstrate compliance with the terms of IDAPA 58.01.01.203. This section of the Rules requires that Interstate demonstrate that emissions from the new HMA drum mix dryer will comply with all applicable emissions standards, and will not cause or significantly contribute to a violation of any ambient air quality standard.

IDAPA 58.01.01.205...... Permit Requirements for New Major Facilities or Major Modifications in Attainment or Unclassifiable Areas

This facility does not emit or have the potential to emit any regulated PSD pollutant at major source threshold levels. Therefore, PSD permitting requirements do not apply.

IDAPA 58.01.01.209.01.c Opportunity for Public Comment

This PTC is subject to the provisions of IDAPA 58.01.01.209.01.c. An opportunity for public comment on the PTC application was provided, in accordance with IDAPA 58.01.01.209.01.c., during which time, comments were received from a citizen. DEQ provide the proposed PTC for a formal public comment period in accordance with IDAPA 58.01.01.209.01.c. The public comments period started from June 1, 2004, and ended on June 30, 2004. Responses to the comments are provided in Appendix E of this statement of basis.

IDAPA 58.01.01.210...... <u>Demonstration of Preconstruction Compliance with Toxic Standards</u>

The TAPs emissions resulting from burning of natural gas, propane gas, No. 2 fuel oil, and used oil in the HMA drum dryer were estimated. Appendix A of this document contains all TAPs emissions from the HMA drum dryer. All TAPs emissions from the dryer were demonstrated to meet the requirements specified in IDAPA 58.01.01.210. Refer to the modeling review memorandum in Appendix C of this document.

IDAPA 58.01.01.212...... Obligation to Comply

Receipt of this PTC does not relieve Interstate from the responsibility to comply with all federal, state, and local rules and regulations.

IDAPA 58.01.01.225...... Permit to Construct Processing Fees

The combined emissions increase from this project is subject to the fee provisions of IDAPA 58.01.01.225, and Interstate was assessed a PTC processing fee of \$7,500.00 for an increase in emissions of 220.52 T/yr. The processing fee was paid May 28, 2004.

IDAPA 58.01.01.577...... Ambient Air Quality Standards for Specific Air Pollutants

Ambient air quality modeling predicts this facility will not cause or contribute to a violation of any applicable ambient air quality standard. The modeling analysis is presented in Appendix C.

IDAPA 58.01.01.625...... Visible Emissions Limitation

Emissions from all stationary point sources in the state of Idaho are required to comply with the opacity standards of IDAPA 58.01.01.625-626, unless exempted under Section 625.01. The HMA drum mix dryer stack at the facility is subject to this standard.

All stationary sources are required to comply with the fugitive dust prevention requirements of IDAPA 58.01.01.650-651.

40 CFR 60 Subpart I..... Standards of Performance for Hot Mix Asphalt Facilities

This subpart is applicable to the HMA plant facility and to the RAP processing system according to 60.90 (a), as follows: "(a) The affected facility to which the provisions of this subpart apply is each hot mix asphalt facility. For the purpose of this subpart a hot mix asphalt facility is comprised only of any combination of the following: dryers, systems for screening, handling, storing, and weighing hot aggregate, systems for loading, transferring, and storing mineral filler, systems for mixing hot mix asphalt, and the loading, transfer, and storage systems associated with emission control systems." Also, per 60.90(b), the HMA plant dryer and the RAP system are a facility that "commences construction or modification after June 11, 1973."

Section 60.92, Standard for particulate matter, states: (a) On and after the date on which the performance test required to be conducted by 60.8 is completed, no owner or operator subject to the provisions of this subpart shall discharge or cause the discharge into the atmosphere from any affected facility any gases which: (1) Contain particulate matter in excess of 90 mg/dscm (0.04 gr/dscf). (2) Exhibit 20 percent opacity, or greater.

The loading, transferring, and storing systems associated with the HMA plant facility are subject to the opacity testing requirement specified in 40 CFR 60.8, 60.92(a)(2), and 60.93(b)(2). 40 CFR 60.93(b)(2) specifies that Method 9 and the procedures in 60.11 be used to determine opacity. Permit Conditions 2.3 and 2.4 incorporate the 40 CFR 60.92 requirements. Permit Condition 2.19 requires testing. Permit Condition 2.21 recommends that a test protocol be submitted prior to testing and Permit Condition 2.22 requires that the test results be submitted to DEQ within 30 days after the date that the testing is concluded.

In addition to the testing required by Subpart I, the facility is required to test the affected facility for particulate emissions and visible emissions at least once every five years.

40 CFR 60 Subpart OOO Standards of Performance for Nonmetallic Mineral Processing Plants

Subpart OOO does not apply to the HMA facility or to the RAP equipment

The section for applicability and designation of affected facility, 60.670 (a)(1), is as follows: "Except as provided in paragraphs (a)(2), (b), (c), and (d) of this section, the provisions of this subpart are applicable to the following affected facilities in fixed or portable nonmetallic mineral processing plants: each crusher, grinding mill, screening operation, bucket elevator, belt conveyor, bagging operation, storage bin, enclosed truck or railcar loading station. Also, crushers and grinding mills at hot mix asphalt facilities that reduce the size of nonmetallic minerals embedded in recycled asphalt pavement and subsequent affected facilities up to, but not including, the first storage silo or bin are subject to the provisions of this subpart."

"(b) An affected facility that is subject to the provisions of subpart F or I or that follows in the plant process any facility subject to the provisions of subparts F or I of this part is not subject to the provisions of this subpart."

Section 40 CFR 60.670(a)(1) above does not apply to the RAP in this PTC. Section 40 CFR 60.670(a)(1) specifically applies to crushers and grinding mills (and subsequent facilities). This permit

application does not include a RAP crusher or grinding mill. It has a lump breaker. The RAP is crushed at a separate facility prior to processing at this facility. The lump breaker at this facility breaks up clumps of conglomerated RAP to a size that is fed onto a conveyor. Oversize stone is rejected, not crushed, by the system. A February 27, 2004, letter from Interstate to DEQ, in which the company submitted additional information for PTC No. P-040101, shows an example of a RAP breaker. That letter is provided in Appendix A of this document. Clearly, the lump breaker is not a crusher, and therefore, Subpart OOO is not applicable to the lump breaker.

In addition, this facility is subject to Subpart I, and, per Subpart OOO (b), Subpart OOO is not applicable to facilities, which are subject to Subpart I.

40 CFR 279 Standards for the Management of Used Oil

Part 279.11 contains specifications for used oil which include allowable levels for arsenic, cadmium, chromium, lead, the flash point, and total halogens. The limit for total halogens is listed at 4,000 ppm maximum. However, used oil containing more than 1,000 ppm total halogens is presumed to be a hazardous waste under the rebuttable presumption provided under § 279.10(b)(1). Such used oil is subject to subpart H of part 266 of this chapter rather than this part when burned for energy recovery unless the presumption of mixing can be successfully rebutted. According to Interstate Concrete and Asphalt Company, the used oil that is used by the facility does not contain total halogens greater than 1,000 ppm, so, as agreed with the facility, the permit limits the total halogens to 1,000 ppm.

Permit Condition 2.9 states that, in accordance with 40 CFR 279.11, used oil burned for energy recovery shall not exceed any of the allowable levels of the constituents and property listed in Table 2.2.

TABLE 2.2 USED OIL SPECIFICATIONS¹

Constituent/property	Allowable level
Arsenic	5 ppm² maximum
Cadmium	2 ppm maximum
Chromium	10 ppm maximum
Lead	100 ppm maximum
Flash point	100 deg. F minimum
Total halogens	1,000 ppm maximum

The specification does not apply to mixtures of used oil and hazardous waste that continue to be regulated as hazardous waste (see 40 CFR 279.10(b)).

² parts per million

This table is based on Table 1 from 40 CFR 279.11, incorporating the 1,000 ppm limit for total halogens as explained above.

5.5 Fee Review

Interstate Concrete and Asphalt Company paid the \$1,000 application fee as required in IDAPA 58.01.01.224 on January 15, 2004.

A permit to construct processing fee of \$7,500.00 is required in accordance with IDAPA 58.01.01.225, because the increase in emissions from the modification was more than 100 T/yr. The \$7,500.00 processing fee was received May 28, 2004.

The Interstate Concrete and Asphalt Company facility is not a major facility as defined in IDAPA 58.01.01.008.10. Therefore, registration fees are not applicable in accordance with IDAPA 58.01.01.387.

6. PERMIT CONDITIONS

This section lists the permit conditions required to demonstrate compliance with emissions and ambient air quality standards.

Permit Condition 2.3 limits PM emissions from the drum dryer stack to the NSPS emissions limit of 0.4 gr/dscf and the opacity to no more than 20% opacity as required by 40 CFR Part 60.92(a)(1).

Permit Condition 2.4 limits the opacity from all other affected facilities to no more than 20% opacity as required by 40 CFR Part 60.92(a)(1).

Permit Condition 2.5 limits CO emissions to 96.2 T/yr. CO is the pollutant emitted in the greatest quantity and its limit establishes the facility's potential to emit.

Permit Condition 2.8 limits the type of fuel that can be burned in the drum dryer burner. The allowable fuels are natural gas, propane, diesel fuel (No. 2 fuel oil), and used oil.

Permit Condition 2.9 limits the concentration of arsenic, cadmium, chromium, lead and total halogens in any used oil the facility may burn. The used oil's flash point is also limited. Total halogens are limited to 1,000 ppm to assure the used oil cannot be classified as hazardous waste.

Permit Condition 2.10 limits the sulfur content in the diesel fuel and used oil to a maximum 0.5% by weight.

Permit Condition 2.11 limits the hot-mix asphalt production of the facility to 1,480,000 T/yr. This limit and Permit Condition 2.15 establish the facility's potential to emit.

Permit Condition 2.15 limits the HMA plant's hours of operation to 3,700 hr/yr.

Permit Condition 2.16 requires the permittee to monitor the pressure drop across the drum dryer baghouse stack once per day when operating to make sure the baghouse is operating according to the manufacturers recommended pressure drop operating range; requires the permit monitor and record the hot-mix asphalt production to demonstrate compliance with Permit Condition 2.11; and requires the permit monitor and record the hours of operation to demonstrate compliance with Permit Condition 2.15.

Permit Condition 2.19 requires that the permittee conduct a performance test to measure PM emissions to demonstrate compliance with Permit Condition 2.3. Testing is required at least once every five years.

Permit Condition 2.20 restricts operations in any PM₁₀ nonattainment area or proposed PM₁₀ nonattainment area. If the permittee wants to operate in one of these areas, a permit allowing such operations is required.

Permit Condition 2.21 requires an analysis of all used to demonstrate that its constituents do not exceed the limits provided by Permit Condition 2.9.

Permit Condition 2.24 requires that the permittee monitor and record the fuel sulfur content (diesel fuel and used oil) on an as-received-basis to demonstrate compliance with Permit Condition 2.10.

7. PUBLIC COMMENT

A public comment period was provided in accordance with IDAPA 58.01.01.209.01.c from June 1 through June 30, 2004. Comments on the proposed permit were provided by a member of the public. Those comments and DEQ's response is provided as Appendix E.

8. RECOMMENDATION

Based on review of application materials, and all applicable state and federal rules and regulations, staff recommend that Interstate Concrete and Asphalt Company in Rathdrum be issued a final PTC No. P-040101 for the new HMA plant. A public comment period on the air quality aspects of the proposed PTC No. P-040101was provided in accordance with IDAPA 58.01.01.209.01.c.

HE/sd

Permit No. P-040101

APPENDIX A

Emissions Inventory

P-040101



Technical Analysis

February 19, 2004

Interstate Concrete & Asphalt, Coeur d'Alene P-040101

Prepared by:

Dan Pitman, Senior Engineer Division of Technical Services

Acronyms, Units, and Chemical Nomenclatures

actma actual cubic feet per minute

CO carbon monoxide

DEQ Department of Environmental Quality

ib/hr pound per hour
NO_X nitrogen oxides
PM Particulate Matter

PM₁₀ Particulate Matter with an aerodynamic diameter less than or equal to a nominal 10 micrometers

SO₂ sulfur dioxide T/yr Tons per year



The purpose for this rmemorandum is to review the emissions estimates provided by Interstate Asphalt & Concrete (Interstate) in a permit to construct application.

PROJECT DESCRIPTION

Interstate is proposing to increase the capacity of a drum mix asphalt plant. Interstate is also proposing to use waste oil and fuel oil in addition to propane and natural gas.

TECHNICAL ANALYSIS

Process Description

Aggregate is heated and dried in a rotating drum. The heated and dried aggregate is then mixed with liquid asphalt cement. Particulate matter emissions from the drum dryer are controlled by a baghouse.

Equipment Listing

CMI PTD-400 Hot mix asphalt plant dryer

Emissions Estimates

The Department of Environmental Quality (DEQ) conducted confirmatory emissions estimates to compare to the emissions estimates supplied by the applicant for a 400-ton per hour drum mix asphalt plant. The applicant proposed an annual production limitation of 1,480,000 tons per year. Both the applicant's and DEQ's emissions estimates are based on EPA AP-42¹, Section 11.1 emissions factors for hot mix asphalt plants. Appendix A contains DEQ's emissions estimates for the drum mix asphalt plant while firing natural gas, number 2 fuel oil and waste oil. Appendix B contains a summary of DEQ's emissions estimates and the applicant's emissions estimates for worst case emissions.

Table 1 gives a summary of the criteria air pollutant emissions estimates for the drum dryer.

Pollutant	PN	PM ₁₀	אס,	SO ₂ "	CO.	VOC'	Pi
Potential Emissions Rute	13.2	9.2	22	23.2	52	12.8	6.0E-3
(It/hr) Potential Emissions							
Rate	24.42	17.02	40.7	42.92	96.2	23.68	1.11E-2

Table 1. Potential Emissions from Drum Dryer

- a) Particulate matter
- b) Particulate matter with an aerodynamic diameter less than or equal to a nominal 10 micrometers
- c) Nitrogen oxides
- d) Sulfur dioxide
- e) Carbon monoxide
- f) Volatile organic compound
- g) Lead

¹ Compilation of Air Pollutant Emissions Factors (AP-42), Fifth Edition, Volume I: Stationary Point and Area Sources, U. S. Environmental Protection Agency, Washington, DC.

Stack Parameter Basis

The applicant provided stack and exhaust gas parameters in the application. An induced draft fan moves the air through the drum mix dryer to the baghouse. Table 2 gives the stack parameters provided in the application.

Table 2. Stack Parameters for Asphalt Plant Dryer

Emissions Unit	(ft)	Stack Diameter (R)	Gas Flowrete (actm)	Stack Temp. (*F)
CMI PTD-400 Hot Mix Asphalt Plant Dryer	30	4.66	63,292	275

Operating Parameters

Operational Factors

Air pollution emissions estimates from the drum dryer are dependent on the rate at which aggregate is processed through the dryer, the type of fuel that is used by the dryer and the type of air pollution control device used. The emissions estimates in this memorandum are based on: an aggregate throughput of 400 tons per hour and 1,480,000 tons per year; the fuel used is either waste oil, natural gas or number 2 fuel oil; and the air pollution control device is a baghouse. Emissions estimates for the drum mix dryer while using natural gas as a fuel can be assumed to be equivalent to emissions that would occur when the dryer is utilizing propane as a fuel.

Metal emissions from the drum mix asphalt plants are the same whether they are processing recycled asphalt pavement (RAP) or normal aggregate (AP-42, Table 11.1-12, footnote a.). For all other pollutants no emissions factors were available dryers while using RAP. AP-42 Table 11.1-10, footnote b, says that tests on processing RAP in drum mix dryers yielded limited data, so the effect of recycled asphalt processing on emissions could not be determined.

DP/sl P-040101

Appendix A Drum Mix Dryer Emissions Estimates

Interstate Concrete and Asphalt

Used Oil Fired Drum Mix Asphalt Plant Dryer With Febric Filter

Hourly Throughput Annual Throughput

400 T/hr 1480000 Arryr

REAL PROPERTY OF THE PARTY OF T	Emission		
	- A	Enterone	Enlace
			TIME
PM (total)	0.033	13.2	24.42
PM-10 (total)	0.023	9.2	17.02
CO	0.13	52	96.2
NOx	0.055	22	40.7
SO ₂	0.058	23.2	42.92
voc	0.032	12.6	23.68
HCf	0.00021	0,084	0.1554
Dioxina*			
2,3,7,8-TCDD	2.10E-13	8.4E-11	1.554E-10
Total TCDD	9.30E-13	3.72E-10	6.882E-10
1,2,3,7,8-PeCDD	3.10E-13	1.24E-10	2.294E-10
Total PeCDD	2.20E-11	6.8E-09	1.628E-08
1,2,3,4,7,8-HxCDD	4.20E-13	1.68E-10	3.108E-10
1,2,3,6,7,8-HxCDD	1.30E-12	5.2E-10	9.62E-10
1,2,3,7,8,9-HxCDD	9.80E-13	3.92E-10	
Total HxCDD	1.20E-11	4.8E-09 1.92E-09	8.88E-09 3.552E-09
1,2,3,4,6,7,8-Hp-CDD	4.80E-12 1.90E-11	7.6E-09	3.552E-08
Total HpCDD	2.50E-11	1E-08	1.85E-08
Octa CDD Total PCDD	7.90E-11	3.16E-08	5.846E-08
Furans*	7.505.77		
2.3.7.8-TCDF	9.70E-13	3.88E-10	7.178E-10
Total TCDF	3.70E-12	1.46E-00	2.738E-09
1,2,3,7,8-PeCDF	4.30E-12	1.72E-09	3.182E-09
2,3,4,7,8-PeCDF	8.40E-13	3.36E-10	
Total PeCDF	8.40E-11	3.36E-08	6.216E-08
1,2,3,4,7,8-HxCDF	4.00E-12	1.6E-09	2.96E-09
1,2,3,6,7,8-HxCDF	1.20E-12	4,8E-10	
2,3,4,6,7,8-HxCDF	1.00E-12	7.6E-10	
1,2,3,7,8,9-HxCDF	8.40E-12 1.30E-11	3.38E-09 5.2E-09	6.216E-09 9.52E-09
Total HxCDF	8.50E-12	2.6E-09	4.81E-09
1,2,3,4,6,7,8-HpCDF 1,2,3,4,7,8,9-HpCDF	2.70E-12	1.08E-09	1.998E-09
Total HpCDF	1.00E-11	4E-09	7.4E-00
Octa CDF	4.80E-12	1.92E-09	3.552E-09
Total PCDF	4.00E-11	1.6E-08	2.96E-08
Total PCDD/PCDF	1,20E-10	4.8E-08	8.88E-06
(Dest Photol. And	1		
Acetaklehyde*	0.0013	0.52	0.962
Acrolein	2.80E-05	0.0104	0.01924
Benzene*	0.00039	0.156	0,2886
Ethylbenzene*	0.00024	0.096	0.1776
Formaldehyde*	0.0031	1.24	2,294
Hexane*	0.00092	0.368	0.6808
	4.00E-05	0.016	0.0296
Isoociane	2.00E-05	0.008	0.0148
Methyl Ethyl Ketone*	0.00013	0.052	0.0962
Propionaldehyde*	0.00016	0.064	0.1184
Quinone*	4.80E-05	0.0192	0.03552
Methyl chloroform	0.0029	1.16	
Toluene"			2,148
Xylene*	0.0002	0.08	0.148

FOR THE STATE OF T	- Emple state 3		
			E TREETON
2-Methykraphthalene	0.00017	6.80E-02	1.26E-01
Acenaphthene	1.40E-06	5.60E-04	1.04E-03
Acenaphthylene	2.20E-06		1.63E-02
Anthracene	3.10E-06	1.24E-03	2.29E-03
	· · · · · · · · · · · · · · · · · · ·		
Benzo(a)anthracene	2.10E-07	8.40E-05	1.55E-04
Benzo(a)pyrene*	9.80E-09	3.92E-06	7.28E-06
Benzo(b)fluoranthene	1.00E-07	4.00E-05	7.40E-05
Benzo(e)pyrene	1.10E-07	4,40E-08	8.14E-05
Benzo(g,h,i)perylene	4.00E-08	1,60E-05	2.96E-05
Benzo(k)/fuoranthene	4.10E-08	1.84E-05	3.03E-05
Chrysene	1.80E-07	7.20E-06	1.33E-04
Fluorantherie	6.10E-07	2.44E-04	4.51E-04
Fluorene	1.10E-05	4.40E-03	8.14E-03
indeno(1,2,3-cd)pyrene	7.00E-08	2.80E-06	5.18E-06
			4.81E-01
Naphthalene*	0.00066	2.60E-01 3.52E-06	6.51E-06
Perylene	8.80E-09		
Phenanthrene	2.30E-05		1.70E-02
Pyrene	3.00E-06	1.20E-03	2.22E-03
Acetone*	0.00083		6.14E-01
Benzaldehyde	0.00011	4.40E-02	8.14E-02
Butane	0.00067	2.68E-01	4.96E-01
Butyraldehyde	0.00016	8.40E-02	1.18E-01
Crotonaldehyde*	8.60E-05	3,44E-02	8.36E-02
Ethylene	0,007	2,80E+00	6.18E+00
Heptane	0.0094	3.76E+00	6.96E+00
Hexans	0.00011	4.40E-02	8.14E-02
isovaleraidehyde	3.20E-05	1.28E-02	2.37E-02
2-Methyl-1-pentene	0.004	1,60E+00	2.96E+00
2-Methyl-2-butene	0.00058	2.32E-01	4.20E-01
3-Methylpentane	0,00019	7.60E-02	1.41E-01
1-Pentene	0.0022	8.80E-01	1,63E+00
n-Pentane	0.00021	8.40E-02	1.55E-01
Valersidehyde	6.70E-05	2.68E-02	4.96E-02
Antimony*	1.60E-07	7.20E-05	1.33E-04
Arsenic*	6.60E-07	2,24E-04	4.14E-04
Berlum*	5.80E-00		
Beryffum"	0.0000		
	·	-	
Cadmium	4.10E-07		
Chromlum*	5.50E-06	2.20E-0	4.07E-03
Cobelf*	2.60E-08	1.04E-0	1.92E-05
Copper	3.10E-00	1.24E-03	2.29E-03
Hexavalent Chromium*	4.50E-07		
Leed	1.50E-0		<u></u>
	······		
Manganese"	7.70E-00		
Mercury*	2.80E-00		
Nickel*	6.30E-05	2.52E-0	4.66E-02
Phosphorus*	2.80E-0		
Silver'	4.80E-07	· · · · · · · · · · · · · · · · · · ·	
Selenium*			
	3.50E-07		
The Num*	4.10E-0		
Zinc*	6.10E-0	2,44E-0	2 4.51E-02

- a) Emission factors are from AP-42 11.1, Hot Mix Asphalt Plants
 b) Pounds per ton
 c) Pounds per hour
 d) Tons per year
 e) IDAPA Toxic Air Pollutant



Natural Gas Fired Drum Mix Asphalt Plant Dryer With Fabric Filter

Hourly Throughput Annual Throughput 400 T/hr 1480000 bir/yr

INTERNATION CONTRACTOR	高速性系统	grad fré est	
PM (total)	0.033	13.2	24.42
PM-10 (total)	0.023	9.2	17.02
co	0.13	52	96.2
NOx	0.026	10.4	19.24
SO ₂	0.0034	1.36	2.516
voc	0.032	12.8	23.68
Hcie	No Data		
Benzene*	0.00039	0.156	0.2886
Ethylbenzene*	0.00024	0.096	0.1776
Formaldehyde*	0.0031	1.24	2.294
Hexane*	0.00092	0.368	0.6808
Isooclane	4.00E-05	1.60E-02	2.96E-02
Methyl chloroform	4.80E-05	1.92E-02	3.55E-02
Toluene*	0.00015	6.00E-02	1.11E-01
Xylene*	0.0002	8.00E-02	1.48E-01
2-Methylnaphthalene	7.40E-05	2,96E-02	5.48E-02
Acenaphthene	1.40E-06	5.60E-04	1.04E-03
Acenaphthylene	8.60E-06	3.44E-03	6.36E-03
Anthrecene	2.20E-07	8.80E-05	1.63E-04
Benzo(a)anthracene	2.10E-07	8.40E-05	1.55E-04
Benzo(a)pyrene*	9.80E-09	3.92E-06	7.25E-06
Benzo(b)fluoranthene	1.00E-07	4.00E-05	7.40E-05
Benzo(e)pyrene	1.10E-07	4.40E-05	8.14E-05
Benzo(g,h,l)perylene	4.00E-08	1.80E-05	2.96E-05
Benzo(k)fluoranthene	4.10E-08	1.64E-05	3.03E-05
Chrysene	1.80E-07	7.20E-05	1.33E-04
Fluoranthene	6.10E-07	2,44E-04	4.51E-04
Fluorene	3.80E-06	1.52E-03	2.81E-03
indeno(1,2,3-cd)pyrene	7.00E-09	2.80E-06	5.18E+06
Naphthaiene*	9.00E-05	3.60E-02	6.66E-02
1 Anhita destain			

AND RESIDENCE OF THE RESIDENCE STREET,	v (4) - (3	· · · · · · · · · · · · · · · · · · ·	The grant was a way
Perylene	8.80E-09	3.52E-06	6.512E-06
Phenenthrene	7.60E-06	3.04E-03	5.62E-03
Pyrene	5.40E-07	2.16E-04	4.00E-04
Butane	0.00067	2.68E-01	4.96E-01
Ethylene	0.007	2.80E+00	5.18E+00
Heptane	0.0094	3.76E+00	6.96E+00
2-Methyl-1-pentene	0.004	1.60E+00	2.96E+00
2-Methyl-2-butene	0.00058	2.32E-01	4.29E-01
3-Methylpentane	0.00019	7.60E-02	1.41E-01
1-Pentene	0.0022	8.80E-01	1.63E+00
n-Pentane	0.00021	8.40E-02	1.55E-01
Antimony ^a	1.80E-07	7.20E-05	1.33E-04
Arsenic*	5.60E-07	2.24E-04	4.14E-04
Berlum*	5.80E-06	2.32E-03	4.29E-03
Beryllium [*]	0	0.00E+00	0.00E+00
Cadmium*	4.10E-07	1,64E-04	3.03E-04
Chromium*	5.50 E-06	2,20E-03	4.07E-03
Cobalt"	2.60E-08	1.04E-05	1.92E-05
Copper ^a	3.10E-06	1.24E-03	2.29E-03
Hexavalent Chromium*	4.50E-07	1.80E-04	3.33E-04
Lead	6.20E-07	2.48E-04	4.59E-04
Manganese*	7.70E-06	3.08E-03	5.70E-03
Mercury*	2.40E-07	9.60E-05	1.78E-04
Nickel ^e	6.30E-05	2.52E-02	4.66E-02
Phosphorus*	2.80E-05	1.12E-02	2.07E-02
Silver*	4.80E-07	1.92E-04	3.55E-04
Selenium*	3.50E-07	1.40E-04	2.59E-04
Thellium*	4.10E-09	1.64E-06	3.03E-06
Zinc*	6.10E-05	2.44E-02	4.51E-02

- a) Emission factors are from AP-42 11.1, Hot Mix Asphalt Plants
- b) Pounds per ton
- c) Pounds per hour
- d) Tons per year
- e) IDAPA Toxic Air Pollutant

interstate Concrete and Asphalt

#2 Fuel Oil Fired Drum Mbx Asphalt (Planst Dryer With Fabric Filter

Hourly Throughput Armuni Throughput

400 T/N 1480000 Janys

and the second second	F-2010 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		SHEROM
		* * *	-3. Shorts
		2	
	0.033	13.2	24,42
PM (total)	0.023	9.2	17.02
PM-10 (total)	0.023	52	96.2
<u> </u>	0.055	22	40.7
NOx	0.011	4.4	8.14
so, .		12.8	23.68
voc	0.032	!#.¥	20,00
HCL'	No Deta	0.484	0.0000
Benzene*	0.00039	0.156	0,2886
Ethylberizene"	0.00024	0,096	0,1776
Formeldehyde*	0.0051	1.24	2.294
Hexane	0.00092	0.368	0,6808
isocciane	4.00E-05	1.80E-02	2.96E-02
Methyl chloroform"	4.80E-05	1.92E-02	3.55E-02
Toksene ³	0.0029	1.18E+00	2.15E+00
Xytene*	0.0002	8.00E-02	1.48E-01
2-Methylnephthelene	0,00017	6.80E-02	1.26E-01
Acenaphthene	1.40E-06	5.60E-04	1.04E-03
Acensphittylene	2.20E-05	5.80E-03	1.63E-02
Anthrecene	3.10E-06	1.24E-03	2.29E-03
Senzo(a)enthracene	2.10E-07	8.40E-05	1.55E-04
Benzo(a)pyrane*	9.80€-09	3.92E-06	7.25E-06
Berzo(b)fluoranthene	1.00E-07	4.00E-05	7.40E-05
Benzo(e)pyrene	1.10E-07	4.40E-05	8.14E-05
Benzo(g,h,!)perylene .	4.00E-08	1.60E-05	2.95€-05
Benzo(k)fluoranthene	4.10E-08	1.64E-05	3.03E-05
Chrysene	1.80E-07		1.33E-04 4.51E-04
Fluoranthene	6,10E-07	2.44E-04 4.40E-03	8.14E-03
Fluoriene	1,10E-05	2.80E-06	5.18E-06
Indeno(1,2,3-od)pyrene	7.00E-09	2.60E-01	4.81E-01
Naphthelene*	0.00065		
Perylene	8.80E-09	3.52E-06	6.51E-06
Phenonthrone	2.30E-05	9.20E-03	1.70E-02
Ругеле	3.00E-06	1.20E-03	2.22E-03
Butene	0.00067	2.88E-01	4.96E-01
Ethylane	0.007	2.80E+00	5.18E+00
Heptane	0.0094	3.76E+00	6.96E+00
2-Mathyl-1-pentens	0.004	1,80E+00	2.96E+00
2-Methyl-2-butene	0.00058	2.32E-01	4.29E-01
	0.00019	7.80E-02	1.41E-01
3-Methylpentane	0.0022	8.80E-01	1,63E+00
1-Persone	0.00021	8.40E-02	1.55E-01
n-Pentane	T 0.00051	<u> </u>	

		M. 1733	50 B.M
Dicodess*			
2.3,7.8-TC00	2.10E-13	8.4E-11	1.854E-10
Total TCDD	9.30E-13	3.72E-10	8.862E-10
1,2,3,7,8-P+CDO	3.10E-13	1.24E-10	2.294E-10
Total PeCIDD	2.20E-11	8.8E-00	1.628E-08
1,2,3,4,7,8-HxCDD	4.20E-13	1.66E-10	3.108E-10
1,2,3,8,7,8-HxCDD	1.30E-12	5.2E-10	9.62E-10
1,2,3,7,8,9-HxCOD	9.80E-13	3.92E-10	7.252E-10
Total HxCDD	1,20E-11	4.8E-00	8.88E-09
1,2,3,4,6,7,8-Hp-CDO	4,80E-12	1,92E-09	3.552E-09
Total HpCOD	1.90E-11	7.6E-00	1.406E-06
Octa COO	2,50E-11	1E-06	1.85E-08
Total PCDD	7.00E-11	3,18E-08	5.846E-06
Furness		Ĺ	
2,3,7,8-TCDF Total TCDF	9.70E-13	3.88E-10	7.178E-10
	3.70E-12	1,48E-09	2.736E-00
1,2,3,7,8-PaCDF	4.30E-12	1.72€-00	
2,3,4,7,8-PeCDF	8.40E-13	3.36E-10	
Total PaCDF	8,40E-11	3.36E-08	
1,2,3,4,7,6-HxCOF	4.00E-12	1.8E-09	
1,2,3,8,7,8-HxCDF	1.20E-12 1.90E-12	4.8E-10 7.6E-10	
2,3,4,6,7,8-Hs:CDF 1,2,3,7,8,9-Hs:COF	8.40E-12		
Total HxCDF	1.30E-11		
1,2,3,4,6,7,8-HpCDF	6.50E-12		
1,2,3,4,7,8,9-HpCDF	2.70E-12		
Total HpCDF	1,00E-11	4E-00	7.4E-09
Octa CDF	4.80E-12		
Total PCDF	4.00E-11		
Total PCDD/PCDF	1,20E-10	4,8E-06	0.88E-08
Antimony*	1.80E-07	7.20E-0	1.33E-04
Arsenic*	5.60E-07	2.24E-04	4.14E-04
Barium*	5.80E-06	2.32E-00	4.29E-03
Beryffum*		0.00	0.00
Cadmium*	4.10E-07	1.84E-0	3.03E-04
Chromium"	5.50E-0	2.20E-0	4.07E-03
Cobelf*	2.60E-00	1,04E-0	1.92E-06
Copper	3.10E-00	1.24E-0	2.29E-03
Hexavarient Chromium*	4.50E-07	1.80E-0	1 3.33E-04
Leed	1.50E-0	6.00E-0	3 1.11E-02
Manganese*	7.70E-00	3.08E-0	5.70E-03
Mercury	2.60E-00	1.04E-0	1.025-03
Nickef	6.30E-0	2.52E-0	2 4.88E-02
Phosphorus*	2.80E-0	1.12E-0	2 2.07€-02
Silver*	4.80E-0	1.92E-0	4 3.55E-04
Seleraum"	3.50E-0		
The flum	4.10E-0	1.84E-0	6 3.03E-06

- a) Emission factors are from AP-42 11.1, Hot Mix Asphalt Plents
 b) Pounds per ton
 c) Pounds per hour
 d) Tons per year
 e) IDAPA Toxic Air Pollutans

Appendix B

Summary of Emissions Estimates

interstate Concrete and Asphelt

Maximum Emissions from Drum Dryer using Natural Gas, #2 Fuel Oil or Waste Oil with Fabric Filter

	1. V. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.				grand d
PM (total)	13.2	Same	2-Methylmaphthalene	6.80E-02	ND
PM-10 (total)	9.2	Seme	Acenephthene	5.80E-04	NO
CO	52	Same	Acenephthylene	8.80E-03	ND
NOx	22	Same	Anthraceme	1,24E-03	ND
SO ₂	23.2	Same	Benzo(a)enthracene	8.40E-05	ND
voc	12.8	Same	Berizo(s)pyrene	3.92E-06	2.00E-04
HCF	0.084	Same	Benzo(b) fluoranthene	4.00E-05	NO
		¢	Benzo(e)pyrene ^d	4.40E-05	NO
Dioxins*	8.4E-11	c	Benzo(g,h,)perylene	1.60E-05	NO
2,3,7,8-TCDD	3.72E-10	č	Benzo(k)fluoranthene	1.64E-05	NO
Total TCDD 1,2,3,7,8-PeCDD	1.24E-10	C	Chrysene	7.20E-05	NO
Total PeCDD	8.8E-09	¢	Fluoranthene	2.44E-04	NO
1,2,3,4,7,8-HxCDD	1.68E-10	¢	Fluorene	4.40E-03	NO
1,2,3,6,7,8-HxCDD	5.2E-10	Č	Indeno(1,2,3-cd)pyrene	2.80E-06	ND
1,2,3,7,8,9+txCDD	3.92E-10	C	Naphthaiene ^e	2.80E-01	ND
Total HxCDO	4.8E-09	£	Perylene	3.52E-06	NO
1,2,3,4,8,7,8-Hp-CDD	1.92E-09	C	Phenanthrene	9,20E-03	NO
Total HpCDD	7.6E-09	C	Pyrene	1.20E-03	ND
Octa CDD	0.00000001	¢	Acetone	3.32E-01	Same
Total PCDD	3.16E-08	C	Benzaldehyde	4.40E-02	ND
Furans [*]		Ç	Butane	2.68E-01	ND
2,3,7,8-TCDF	3.88E-10	· c	Butyreidehyde	6.40E-02	ND
Total TCDF	1.48E-09	C	Crotonaldehyde ⁶	3.44E-02	Same
1,2,3,7,8-PeCDF	1.72E-09	¢	Ethylene	2.80E+00	ND
2,3,4,7,8-P+CDF	3.36E-10	C	Heptane	3.76E+00	Seme
Total PeCDF	3.36E-08	€	Hexamal	4.40E-02	ND.
1,2,3,4,7,8-HxCDF	1.6E-09	<u>c</u>	isovalersidehyde	1.28E-02	ND
1,2,3,8,7,8-HxCDF	4.8E-10 7.6E-10	<u> </u>	2-Methyl-1-pentene	1.60E+00 2.32E-01	ND ND
2,3,4,6,7,8-HxCDF	3.36E-09	€ .	2-Methyl-2-butene	7.60E-02	ND ND
1,2,3,7,8,9-HxCDF	5.2E-09	č	3-Methylpentane 1-Pentene	8.80E-01	NO
Total HxCDF	2.6E-09	Č	n-Pentane	8.40E-02	Same
1,2,3,4,8,7,8-HpCDF	1.08E-09	¢	Valeraldehyde	2.68E-02	Serne
1,2,3,4,7,8,9+4pCDF	4E-09	ε	Antimony [®]	7.20E-05	- · · · · · · · · · · · · · · · · · · ·
Total HpCDF	1.92E-09	¢	Amenic	2.24E-04	Seme
Octa CDF	1,6E-08	c	Barkern ^a :	2.32E-03	NO
Total PCDF	4.8E-08		Beryllium .	0.00E+00	Same
Total PCDD/PCDF	4,00,00			4	
			Cadmium ^a	1.64E-04	2.00E-04
Aceteldehyde ⁴	0.52	Seme	Chromium	2.20E-03	Same
Acrolein	1.04E-02	Same	Cobsit*	1.04E-05	0
Senzene ^d	0.156	Seme	Copper	1.24E-03	Same
Ethylbenzene*	0.096	Same	Hexavalent Chromlum ^d		2,00E-04
Formaldehyde ^d	1.24	Seme	Lead	6.00E-03	
Hexane*	0.368	Seme	Manganese*	3.08E-03	Seme
soctane	1.60E-02	Same	Mercury	1.04E-03	Same
Methyl Ethyl Ketone	800.0	Same	Nickel ^a	2.52E-02	
Propionaldehyde*	0.052	Same	Phosphorus ⁴	1.12E-02	
Quinone ⁴	0.064	Same	Silver	1.92E-04	
Methyl chloroform	1,92E-02	Same	Selenium ⁶	1.40E-04	· · · · · · · · · · · · · · · · · · ·
	1.16E+00	Same	Thelium*	1.64E-06	
Tokiene			Zinc		
Xylene ^d	8.00E-02	Same	14. A. P.	2.44E-02	Same

- a) Emission estimates made by DEQ using AP-42, Section 11.1 Emissions Factors
 b) Emission estimates provided in the application received on January 26, 2004
 c) Applicant determined that combined dioxin and furan emissions to compare to the todic increment listed in IDAPA 58.01.01.586 is 1.23E-8 pounds per hour
- d) IDAPA Toxic Air Pollutent
- ND Not Determined



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P-040101

January 23, 2004

Bill Rogers
Idaho Dept. of Environmental Quality
1410 N. Hilton
Boise, ID 83706

Subject: Permit to Construct 55-00048 Modification

Dear Mr. Rogers,

I have enclosed two copies of the request to modify along with a CD-Rom of the Modeling Files for our existing plant site. This modification will allow us to replace the existing asphalt plant with a plant capable of burning Spec-Oil and the use of RAP.

We respectfully request that our Permit to Construct be modified to accommodate the above. Please contact me at 765-1144 if you need additional information to make the requested revision to our permit.

Sincerely,

Corky Witherwax Aggregate Sales/

Environmental Manager

JAN 2 6 2004

Department of Environmental Curally
Blade Alt Program



ETE AND ASPHALT COMPANY - W. 845 KATHLEEN - COEUR D'ALENE, 10 83016 7009652 VENDOR NAME CHECK NUMBER 7009652 State Of idaho rauova na RETAINAGE PREVIOUS BALANCE DESCRIPTION GROSS AMOUNT DISCOUNT DATE ENCC permit app fee Jensen HMA 1,000.00 0.00 0.0 0.00 1,000,00 0.00 1/14/0 1/2004 RECEIVED JAN 2 6 2004 DISCOUNT PREVIOUS **GROSS AMOUNT** BALANCE OR NO 0.00 1,000.00 1,000,00 0.00 0.00 23358

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5 KATHLEEN CORLINGWALENE ASPENDS

DATE CHECK NO. AMOUNT

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AUTHORIZED BONATURE

Interstate Concrete and Asphalt Company Asphalt Plant Rathdrum, Idaho

Air Quality Permit Application Modification Wyoming Plant Permit No. 55-00048

Aspen File: ICA03117

Prepared for:

Interstate Concrete and Asphalt Company 845 West Kathleen Avenue Coeur d'Alene, Idaho 83814

Prepared by:

Aspen Consulting & Engineering, Inc.
P.O. Box 4822
Helena, Montana 59604
(406) 457-5188

JAN 26 2004 Department of Environmental Commen

January 19, 2004

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1.0 INTRODUCTION

Interstate Concrete and Asphalt Company (Interstate) owns and operates an asphalt plant in Rathdrum, Idaho known as the Wyoming Plant. Interstate is requesting an air quality Permit to Construct modification for this facility.

The Wyoming Plant currently operates a Gencor Industries/10332, drum mix, natural gas-fired hot mix asphalt plant dryer. The maximum production rate of the dryer is 300 tons per hour of asphalt. This facility is currently restricted to 5,500 hours of operation per year.

A concrete batch plant and a rock crushing plant are also located at the Wyoming Plant facility. The concrete batch plant is currently limited to 1,752,000 cubic yards per any consecutive 12-month period and the rock crushing plant is limited to 831,338 tons per year per any consecutive 12-month period.

1.1 PROPOSED PERMIT MODIFICATION

The existing permit is now listed as owned by Central Pre-Mix. Interstate wishes to change the permit owner name to Interstate Concrete and Asphalt Company. Both Central Pre-Mix and Interstate are owned by CPM Development Corporation. Therefore, the name change should be administrative.

Interstate proposes to replace the existing 300-ton per hour hot mix asphalt plant dryer with a 400-ton per hour CMI PTD-400 drum mix dryer with baghouse control. Interstate also proposes to remove the current primary crusher and replace it with a 500-ton per hour portable crusher, which will be located at the Wyoming Plant on an as needed basis and be controlled by water spray.

Interstate also proposes to include the use of recycled asphalt pavement (RAP) equipment. RAP equipment will allow Interstate to substitute RAP for cold aggregate.

Although the percentage of RAP used will vary, Interstate plans an equal swap of RAP for cold aggregate. Therefore, no particulate emissions increase will occur.

Included in the RAP process are an additional bin, a lump breaker (an enclosed low energy rotor arrangement that breaks up the weak lumps that tend to form in a crushed RAP pile), and two conveyors.

Also, Interstate proposes to burn waste oil, fuel oil, and natural gas as fuel for the asphalt plant dryer. The proposed waste oil fuel is sold under the generic name "On-Spec" oil.

On-Spec oil meets the used oil specifications outlined in Chapter 279 of the Code of Federal Regulations, Subpart B (279 CFR, Subpart B).

Interstate requests the permit be modified to limit the total tons of hot-mix asphalt produced to 1,480,000 tons of HMA during any calendar year to avoid the facility becoming a major source under the Title V operating permit program. This amount of HMA equates to of 3,700 hours per year at maximum production.

Interstate does not propose to change the existing throughput limitations for the concrete batch plant or the rock crushing plant.

Idaho Department of Environmental Quality (DEQ) Standard Permit to Construct application forms are provided in Appendix A. Facility maps are provided in Appendix B.

1.2 PROCESS DESCRIPTION

The asphalt plant has a front-end loader to transfer stockpiled aggregate to five cold feed bins. Aggregate is dispensed from the bins onto slow moving feeder conveyors, sorted by a scalping screen for proportioned size gradations, and finally introduced to a drum mix dryer. Interstate is seeking to allow this drum dryer to burn used oil, fuel oil, and natural gas.

Aggregate travels through the rotating drum counter-current to the heating media. The material is then heated and dried and mixed with liquid asphalt cement. The resulting hot mix asphalt is then conveyed to hot storage bins until it can be loaded into dump trucks for transport off site. Figure 1 provides a general process flow diagram.

The concrete batch plant receives raw materials at the site by truck and are then dumped onto storage piles or conveyed into storage silos. Sand, course aggregate, cement, and fly ash are stored site in silos. These raw materials are combined to form the final concrete product.

Upon demand for concrete, the raw materials are weighed and dumped into a cement truck in the appropriate proportions. Water is added and the slurry is mixed and prepared for off-site delivery of the final product.

The rock crushing plant's quarried stone is dumped into a hopper feeder that feeds the facility's primary crusher. Reject material from the primary crusher is conveyed to the stacker scalp pile. Crushed material is conveyed to the primary screen and then conveyed to one of two secondary crushers. Stone is again crushed and sent via conveyor to additional screens. The tertiary screens select and convey product-sized material to loadout bunkers and return over-sized material to be recrushed in tertiary crushers until product-sized material is produced.

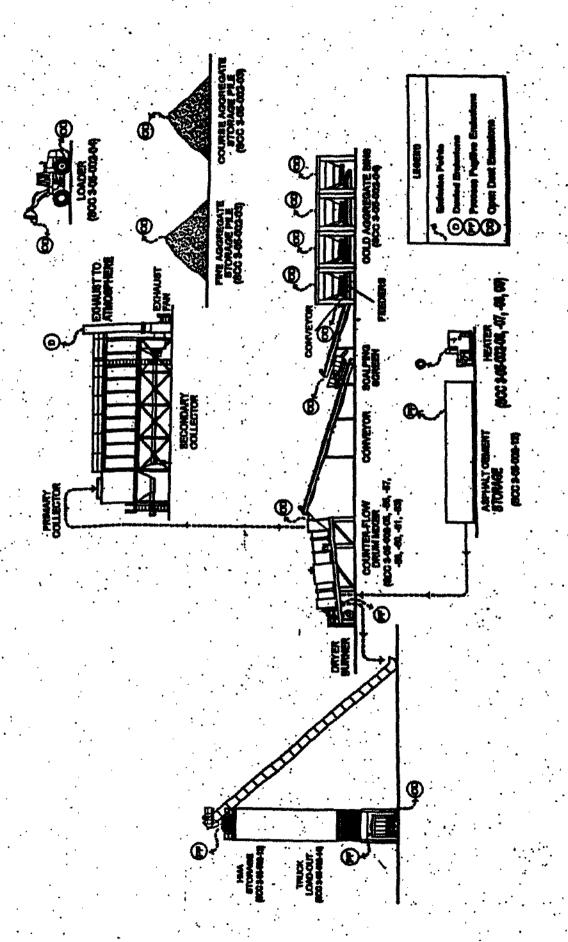


Figure 1. General process flow diagram

2.0 EMISSIONS INVENTORY

Emissions were calculated for both criteria and toxic pollutants. The following sections describe the methodologies, references, and results.

2.1 CRITERIA POLLUTANTS

Emissions estimates were calculated for the following criteria pollutants: Nitrogen Oxides (NO_x), Carbon Monoxide (CO), Sulfur Dioxide (SO₂), Volatile Organic Compounds (VOC), Particulate Matter (PM), and Particulate Matter with an aerodynamic diameter of less than 10 microns (PM₁₀).

The EPA document AP-42, Section 11.1 emission factors (December 2000 edition) for Hot-Mix Asphalt Plants was used for estimating emissions of the criteria pollutants. Emission factors were chosen for drum plants equipped with a fabric filter utilizing the worst-case factor for natural gas, waste oil (estimate for used oil), or fuel oil. In some cases, the emission factors were the same regardless of fuel type. PM and PM₁₀ emission factors include both the filterable and condensable fractions.

Emission totals, in tons per year, were based on a restriction of 1,480,000 tons per year of HMA. Hourly emission rates in pounds per hour (lb/hr) were determined using the proposed maximum production rate of 400 tons per hour.

Since the rock crushing plant and concrete batch plant emissions restrictions are proposed to remain the same, no change from the current existing permitted levels is expected.

An internet search for toxic emission factors did not reveal any information regarding the use of RAP materials in HMA plant dryers, and therefore the toxic emissions are assumed not to change due to the use of RAP.

Table 2-1 below presents a summary of the criteria pollutant emissions inventory.

Interstate requests the current permitted allowable emission limits be modified to reflect the emission levels as shown in Table 2-1. A more detailed emissions inventory spreadsheet is included in Appendix C.

TABLE 2-1 CRITERIA POLLUTANT EMISSIONS SUMMARY INTERSTATE CONCRETE AND ASPHALT WYOMING FACILITY

Pollutant	Emissions (tons/year)
NO _x	40.7
co	96.2
SO₂	• 42.9
VOC	23.7
PM ₁₀	77.2

Notes:

NOx

Nitrogen Oxides

CO

Carbon Monoxide

SO₃

Sulfur Dioxide

PM₁₀

Volatile Organic Compounds
Particulate Matter (aerodynamic diameter < 10 microns)

2.2 TOXIC AIR POLLUTANTS

Toxic air pollutants were estimated using AP-42, Section 11.1 emission factors (December 2000 edition) for Hot-Mix Asphalt Plants. Only emission factors for toxics listed in IDAPA 58.01.01.585 and 586 were selected from AP-42. The worst-case emission factors were chosen from natural gas, waste oil (estimate for used oil), or fuel oil factors. In some cases, the emission factors were the same regardless of fuel type.

Polycyclic organic matter (POM) and poly-aromatic hydrocarbons (PAHs), were determined as equivalent Benzo(a)pyrene. As noted by IDAPA 58.01.01.586, the emission factors for the following PAHs were first summed and then added to the

emission factor for Benzo(a)pyrene to determine if emission levels of PAHs were within acceptable limits:

- > Benzo(a)anthracene
- > Benzo(b)fluoranthene
- > Benzo(k)fluoranthene
- > Dibenzo(a,h)anthracene
- Chrysene
- > Indeno(1,2,3-cd)pyrene

Emission estimates for toxics are calculated to determine if the toxic pollutants resulting from the proposed facility modification will be within acceptable levels as provided for in IDAPA 58.01.01.585 and 586. This rule exempts specific toxics if they are below the screening emissions level (EL) or if they are below the acceptable ambient concentration (AAC) or acceptable ambient concentration for carcinogens (AACC) as prescribed by this rule.

Table 2-2 below presents an emissions summary for toxic air pollutants. Compounds listed in bold signify that the pound per hour emission rate is above the EL for that compound. These compounds are shown to be below the AACs or AACCs in Section 3.0 of this document.

TABLE 2-2 TOXIC AIR POLLUTANT EMISSIONS SUMMARY INTERSTATE CONCRETE AND ASPHALT WYOMING FACILITY

Emissions Factor (lb/ton)	Emissions (lb/hr)	Idmbe E.L. (fb/hr)
3.09E-12	1.23 E-0 9	1.50 E-10
0.0013	6.5200	0.0036
0.00083	0.3320	119.00
2.60E-05	0.0104	0.0170
1.80E-07	0.0001	0.033
5.60E-07	0,0002	1.50E-06
0.00039	0.1560	0.0008
2.10E-07	•.	0.000
· 5.48E-07	0.9002	2.00E-06
1.00E-07 .	_	***************************************
4.10E-08		•
0	o	2.80E-05
4.10E-07	G.0002	3.70E-06
5.50E-06	0.0022	5.60E-07
1.80E-07	· •	*
2.60E-08	0.0000	3.3 OE-03
3.10E-06	0.0012	1.30E-02
8.60E-05	0.0344	0.380
0.00024	0.0960	29.00
0.0031	· · · · · ·	0.00051
0.00021	0.0840	0.0031
0.0094	3.7600	109.0
0.00092		12,000
4.50E-07		5.60B-07
7.00E-09		J.GOD.G/
4.00E-05	0.0160	33 300
7.70E-06		23.300
2.60E-06		6.70E-02
1		3.006-03
1 1	'	127.000
· •		39.300
1		2.70E-05
1 i		118.000
1 1	1	7.00E-03
1 1	,	0.0287
	(Ib/ton) 3.09E-12 0.0013 0.00083 2.60E-05 1.80E-07 5.60E-07 0.00039 2.10E-07 5.48E-07 1.00E-07 4.10E-08 0 4.10E-08 0 4.10E-08 3.10E-06 1.80E-07 2.60E-08 3.10E-06 8.60E-05 0.00024 0.0031 0.00021 0.0094 0.00092 4.50E-07 7.00E-09 4.00E-05 7.70E-06	(Ib/ton) (Ib/hr) 3.09E-12 1.23E-89 0.0013 0.5200 0.00083 0.3320 2.60E-05 0.0104 1.80E-07 0.0001 5.60E-07 0.0002 0.00039 0.1560 2.10E-07

TABLE 2-2 (CONTINUED) TOXIC AIR POLLUTANT EMISSIONS SUMMARY INTERSTATE CONCRETE AND ASPHALT WYOMING FACILITY

Pollutant	Emissions Factor (lb/ton)	Emissions lb/ar	Idaho EL (lb/hr)
Sekenium	3.50B-07	0.0001	1.30E-02
Silver	4.80E-07	0.0002	7.00E-03
Thallium	4.10E-09	0.0000	7.00E-03
Toluene	0.0029	1.1600	25.000
Valeraldehyde	6.70E-05	0.0268	11.700
Xylene	0.0002	0.0800	29.00
Zinc	6.10E-05	0.0244	6.67E-01

Notes

Compounds in bold signify that the compound exceeds the allowable EL.

ISM IDADA Pounds per Hour

**

Total PAHs are considered as equivalents of benzo(a)pyrene. Emission Factors for the compounds with a "*" in the Idaho EL column are added to POMs as equivalent Benzo(a)pyrene.

3.0 SCREEN MODELING ANALYSIS

Modeling of the dryer stack emissions was completed using the EPA-approved SCREEN3 air dispersion model. SCREEN3 is a conservative model that uses worst-case meteorological data and calculates a maximum 1-hour average ambient concentration.

3.1 MODEL INPUT PARAMETERS

Model inputs for stack height, flow, and temperature were provided by Interstate. The dryer stack is a rectangular stack measuring 43 by 57 inches. Since the model requires a diameter input, the equivalent diameter was determined based on an equivalent stack cross-sectional area. Only flat terrain was considered. Model input parameters are listed below:

Stack Height:

30 feet

Stack Flow:

63,292 actual cubic feet per minute (acfm)

Stack Diameter:

4.655 feet

Stack Temperature:

275 degrees Fahrenheit

Emission Rate:

1 pound per hour (lb/hr)

Ambient Temperature:

68 degrees Fahrenheit

3.2 MODEL RESULTS

The SCREEN3 model run using the above-listed parameters estimated a maximum hourly ambient concentration of 1.988 micrograms per cubic meter (µg/m³). The maximum hourly ambient concentration of each individual compound in the ermissions inventory is determined by multiplying the corresponding emission rate in lb/hr by the modeled result of 1.988 µg/m³. Since the modeled concentration was determined on a basis of 1 lb/hr, this calculation is appropriate. Screen model output is provided in Appendix D.

3.3 COMPARISON TO ACCEPTABLE AMBIENT CONCENTRATIONS

AACs and AACCs were reviewed for all compounds that exceeded their ELs. AACs are based on a 24-hour averaging period and AACCs are based on an annual averaging period. The SCREEN3 1-hour modeled concentrations were converted to 24-hour and annual averages using the methods described in IDAPA 58.01.01.210(i). The emissions inventory was developed based on pollutant grouping rather than carcinogen/non-carcinogen groupings. Therefore AACs and AACCs were combined into one table.

As shown below in Table 3-1, all pollutants reviewed are below their respective AAC or AACC except for formaldehyde. A refined modeling analysis is presented in Section 4.0, and results of the analysis showing compliance with the formaldehyde AACC are presented in Section 5.0.

TABLE 3-1 TOXIC AIR POLLUTANT MODELED CONCENTRATIONS INTERSTATE CONCRETE AND ASPHALT WYOMING FACILITY

Pollutant	Medeled 1-hour Concentration (µg/m²)	Medeled 24-hour Concentration (µg/m²)	Modeled Annual Concentration (µg/m²)	Idahe AAC/ AACC (µg/m²)
2,3,7,8 - TCDD	2.91E-09		3.79E-19	2.20E-08
Acetaldehyde	1.2246		6.72E-02	0.45
Arnenic	0.00053	0.00021	· · ·	0.23
Benzene	0.3674		6.05E-03	0.12
Benzo(a)pyrene**	0.00052	0.00021		0.0003
Cadmium	0.00039	0.00015		0.56
Chromium	0.0052	0.9021		0.0830
Formaldehyde	2.9202	· ·	3.82E-01	0.077
на	0.19782	0.079128	·	375
Hexavalent chromium	0.00042	0.00017	, ,	0.083
Nickel	0.0593	0.0237		4.2
Phosphorus	0.0264	0.0106	, .	5
Propionaldehyde	0.1225	0.048984		21.5
Quinone	0.1507	0.060288		20

Notes:

g/m² Micrograms per Cubic Meter

3.4 NATIONAL AMBIENT AIR QUALITY STANDARDS

A source cannot be modified or constructed in an attainment area if the change would cause or contribute to a violation of the National Ambient Air Quality Standards (NAAQS). The 1-hour averages modeled for each criteria pollutant were converted to the appropriate 3-hour, 8-hour, 24-hour, and annual averages where appropriate.

Averages were calculated by multiplying the 1-hour SCREEN3 concentration by the appropriate factors listed in EPA's, "Screening Procedures for Estimating the Air Quality Impact of Stationary Sources, Revised." Concentrations of criteria pollutants versus the appropriate NAAQS for each pollutant are presented in Table 3-2.

TABLE 3-2 MODELED CONCENTRATIONS AND NAAQS INTERSTATE CONCRETE AND ASPHALT WYOMING FACILITY

Pollutant	Modeled 1-hour Concentration (µg/m²)	Modeled Adjusted Concentration (µg/m³)	NAAQS Averaging Period	Idaho Background Concentration (µg/m²)	Final Medeled Concentration (µg/m²)	NAAQS (µg/m²)
NOx	52	4	Annual	17	21	100
•	127	122	1-hour	3,600	3,722	40,000
œ`.	122	86	8-hour	2,300	2,386	10,000
	•	49	- 3-hour	· 34	83 .	1,300*
SO2	55	22	24-hour	26	48	. 365
	, , , , , , , , , , , , , , , , , , ,	4	Annual	8	12	· 80
Ozone (as VOC)	30	· 21	8-bour		21	157
PM-10	Net Emissions I	ecrease. No mo	deling required	for PM10 accordi	ng to Idaho Mode	ling Guiden

Notes:

Secondary Standard

NOx

Nitrogen Oxides Carbon Monoxide

CO SO₂ VOC

Sulfur Dioxide Volatile Organic Compounds

PM₁₀ µg/m Particulate Matter (aerodynamic diameter < 10 microns)

Micrograms per Cubic Meter

A modeling analysis for PM₁₀ was not performed because according to Idaho emissions modeling guidance, permit modifications that propose a net emissions increase of less than 1 ton per year do not require modeling. This proposed facility modification provides a net emissions decrease for PM₁₀.

The modeled concentrations for all criteria pollutants are less than the NAAQS.

4.0 REFINED MODELING ANALYSIS

This section describes the model selected, receptor grid development, meteorological data used, and terrain data used. The refined modeling analysis is being performed to show compliance with the formaldehyde AACC.

4.1 AIR DISPERSION MODEL SELECTION

The EPA approved Industrial Source Complex (ISC3) model was chosen for this refined modeling analysis. ISC3 is a steady-state Gaussian plume model that considers simple and complex terrain.

4.2 RECEPTOR GRID SPACING

Receptors were placed along the facility fence line at 50-meter intervals. A Cartesian receptor grid was developed outside the fence line boundary. Receptors were placed at 100-meter spacing for a distance of 1 kilometer (km) from the fence line. Receptors were placed at 250-meter spacing for distances of 1 km to 3 km from the fence line. Receptors were placed at 500-meter spacing for distances of 3 km to 10 km from the fence line.

All receptors were placed using Universal Transverse Mercator (UTM) coordinates.

4.3 RECEPTOR AND SOURCE ELEVATIONS

Receptor and emission source elevations were determined using United States Geological Survey (USGS) 7.5-minute series (1:24,000 scale) digitized maps. The Coeur d'Alene, Hayden, Post Falls, and Rathdrum, Idaho quadrangles, and the Liberty Lake and Newman Lake, Washington quadrangles in USGS's digital elevation model (DEM) file format were used.

4.4 METEOROLOGICAL DATA

Five years (1987, 1988, 1989, 1990, and 1991) of meteorological data were used in this modeling analysis. Surface and Upper air meteorological data were obtained from Spokane, Washington (Met Station #24157).

5.0 REFINED MODELING METHODOLOGY AND RESULTS

Refined modeling of the dryer stack emissions was performed to show compliance with the formaldehyde AACC. Formaldehyde was the only compound above the AAC or AACC for the proposed dryer stack.

5.1 REFINED MODELING METHODS

The hourly emission rate for formaldehyde, based on AP-42 emission factors (presented in Section 2.0) is 1.24 pounds per hour. However, since Interstate proposes to limit facility production to 3,700 hours per year, and the AACC for formaldehyde is based on an annual concentration, the pound per hour emission rate was adjusted to reflect less than full year of operation.

The adjusted emission rate was used in the refined modeling analysis for formaldehyde and is equal to the proposed hours of operation (3,700) divided by the number of hours in a year (8,760), times the hourly emission rate (1.24 lb/hr). The adjusted emission rate used in the modeling analysis for formaldehyde is therefore 0.524 pounds per hour.

All other dryer stack input parameters used in the SCREEN3 model (as presented in Section 3.1) were used in the refined modeling analysis. Building downwash was not considered since no buildings were within the area of the stack that would affect the stack plume. The rural option was chosen for this modeling analysis.

5.2 REFINED MODELING RESULTS

The refined modeling analysis of the proposed dryer stack showed that the annual concentration for formaldehyde was below the AACC. The receptor (507,371E, 5,291,654N) in the 1990 model year was the predicted annual high concentration for all years modeled and is located approximately 250 meters to the northeast of the facility. Table 5-1 presents the results. A printout of the refined modeling results is provided in Appendix E. Also, two copies of all modeling files are provided in electronic format on CD-ROM.

TABLE 5-1
FORMALDEHYDE
MODELED CONCENTRATIONS
INTERSTATE CONCRETE AND ASPHALT
WYOMING FACILITY

Model Year	Modeled Emissions (lb/kr)	Emissions UTM Coordinates Concentration		idaho AACC (µg/m²)
. 1987		507,471E., 5,291,754N	0.0252	, .
. 1988	· .	507,471E , 5,291,754N	0.0316	,
1989	0.524	507,371E , 5,291,654N	0.0261	0.077
1990		507,371E , 5,291,654N	0.0337	
1991	<u> </u>	507,371E , 5,291,754N	0.0238	

Notes: µg/m² Micrograms per Cubic Meter

6.0 CONCLUSIONS

The proposed burning of used oil or fuel oil in the drum dryer at Interstate's Wyoming Plant can be allowed in accordance with Idaho's Air Quality Regulations. As proposed, Interstate may burn natural gas, used oil, or fuel oil at a production rate of 400 tons per hour of HMA for 3,700 hours per year, not exceeding 1,480,000 tons of HMA produced per calendar year. With these restrictions, Interstate will remain a minor source, meet the toxic air pollutant AACs/AACCs, and not cause or contribute to a violation of the NAAOS.

APPENDIX A APPLICATION FORMS



STATE OF IDAHO DEPARTMENT OF ENVIRONMENTAL QUALITY

APPLICATION TO CONSTRUCT AN AIR POLLUTION EMITTING FACILITY (IDAPA 58.01.01.200-.225)

SECTION 1: GENERAL INFORMATION

COMPANY AND DIVISION NAME Inter	state Concret	e and Asphalt	Company	•		
MALING ACCRESS 845 W. Kathleen	St. COUN	Y Kootenal	,	· ·	JIME BARLOYEES 4	
Coeur d' Alene state ide	aho zeco	e 83815		iebych na	(208) 765-1144	
PERSON TO CONTACT Corky Witherw				ronmental I	Manager	1
EXACT PLANT LOCATION (IDENTIFY LOCALITY B805 W. Wyoming Ave., 0.5 miles	west of High	TM COORDINATES I IWBY 41, Rath	<i>Francium</i> drum, ID. U	JTM Coord	inetes (507,100E, 5,291,110N)
GENERAL NATURE OF BUSINESS AND IGNOS OF	PRODUCTS A	sphelt Plent, R	ock Crushi	ng Plent, e	nd Batch Concrete Plant	
, REASON FOR APPLICATION	00	ALL FACILITIES WITH VITROL OR UNDER CO AIRL IF HONE, BOST	MAKON CONTRO			
permit to construct a new facility		•	•			
permit to modify an existing sou permit number 55-00048	rce	NAME	LOCATION			
permit to construct a new source	•	oncrete Batch	Plant #05	5-00049	Coeur d'Alene	
at an existing facility		Portable Wash Plant #777-00076 Coeur d'Alene Asphalt Plant #055-00036 Hayden				
change of owner or location		ortable Crush			Heyden	
permit number 55-00048 current owner Central Pre-M		sphelt/Concrt Sphelt Plant (7-00048	Sandpoint Blanchard	
& ESTIMATED CONSTRUCTION START DATE S	pring 2004		ESTANATED (COMPLETION DA	Spring 2004	-
10. NAME AND TITLE OF OWNER OR PERPONSIE	EOFFICIAL C.	Patrick McFar	iane, Presi	dent		•
11. In accordance with IDAPA 58.01.1 certify based on information and belitrue, accurate, and complete.	01.123 (Rules i of formed after	or the Control o reasonable inq	f Air Pollution uiry, the state	n in Idaho), ements and	C. Patrick McFarlane Information in the document are	1
SIGNATURE C. Stud Mc	Jalan	,		DATE	1/25/04	

The following information, at a minimum, must be included in the application package in order for the application to be determined complete:

- A scaled plot plan clearly showing property boundaries and stack and building locations;
- All calculations and essumptions used to estimate emissions;
 - Manufacturer a guarantees for stated control efficiencies of all control equipment;
- A description of potential fugitive emissions;
- A namelive description of the facility and the process from feed material in to final product out;
- A process flow diagram; and
- Any other information required by the DEQ to determine the application complete.

ITATE OF IDAHO UPPLICATION TO CONSTRUCT AN AIR POLLUTION EMITTING FACILITY

SECTION 2: FUEL-BURNING EQUIPMENT (complete a separate page for each unit)

				1		······································	6. HEAT UE	· .	
EQUIPMENT HANDFACTUR	ER AND		3. RATED HEAT	1	RMER UNIT		1		•
MODEL NUMBER			NEUT CAPACITY	I	(use code)		% process		% space healing
CMI PTD-400 A	sphalt F	Plant Dryer	120 MMBtu	in 1	·		100		•
PLEL DATA				1	NTROL ECUPMENT		1		
		Primary		1 .		Primary	Second	•	٠.
fuel type (use o	ode)	01	02 (#2)	type	Begho	US6	None	· · · · · · · · · · · · · · · · · · ·	
percent sulful		**************************************		manufact		405			
percent seh		 		[mber RA3-				
percent nitroge	in .	<u></u>		% efficier	ncy 0.04_1	r/decf	<u> </u>		• •
percent carbon	1						v		•
percent hydrog)en			 1	GLANWITED	yes	<u>X</u> no	•	•
percent moist.	n.e	<u></u>		(Include gue	-				•
heat content				-	crubbers:				
(percent by we	ight or vo	karne)		1	er flow				
				- pre	seure drop	ļ	ICHES OF W	intel.	
PLUS, CONSUMPTION		Dimen	Secondary	for begin					•
		Primary	Secondary	IOT DESCRIPT	cioth retto <u>uni</u>	KNOWN	•		
Maximum em	punt	120 mcf	1		ssure drop		oches of w	entar	
burned/hour				┪ ‴	arup		,,,		
Normal amou	TR.			10. STACK OR	EIGHALIST DATA			,	
burned/year						Stack	D Dryer		
Fly ash rein	tacelon?	yes no	n.a.		•		pht 30		ı ı
PHY MAIL FRAME				1 :	ŧ		ter 43" X	57"	R
Q 27 11 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2							me_63,29		acim
· Hours per day	•	12		•			ure 275		F
Days per wer		7 .		l	•		***************************************		•
Weeks per y	1 1	- Se	, , , , , , , , , , , , , , , , , , ,		eperate page	for each	stack if me	ets elqith	cke or vente
		26		are used)		•			
				are used)		······································	**	*******	
1. CRITERIA POLLUTANT	estimated !	94574746							
Particulates	. 9,2	lb/hri 17	7,02 tons/yr	_ ` N	rogen cides	22.0	lb/hr_	40.7	tons/yr
Sulfur dioxide	23.2		2.92 tone/yr		elatile organic	12.8	To/her	23,7	tonsýr
Carbon monoxide	52.0	Ib/hr 9	6.2 tonsyr		ompounds .		•		
<u>.</u>			(include calc	ulations and a	ssumptions)			············	
PUEL CODES			•	BURNER CO					
1. Neturni gas		,		1. Spread			,		rieed stoker
2. Oil (apecify AST	M grede n	umber)		i i	r traveling grai	ie _.		_	entially fired
3. Wood (specify o	hips, bark	, shevings		3. Hand fir	ed		₹ .	9. Hortz	ontally fired
sender dust				4. Cyclone	fumace			10. Oth	r (specify)
4. Cosi (specify bit	uminous, i	untrecite, lignite)	5. Wet bot	tom (pulverize	ed coel)		٠	•
5. Other (specify)				6. Dry bot	om (pulverize	d coal)		•	

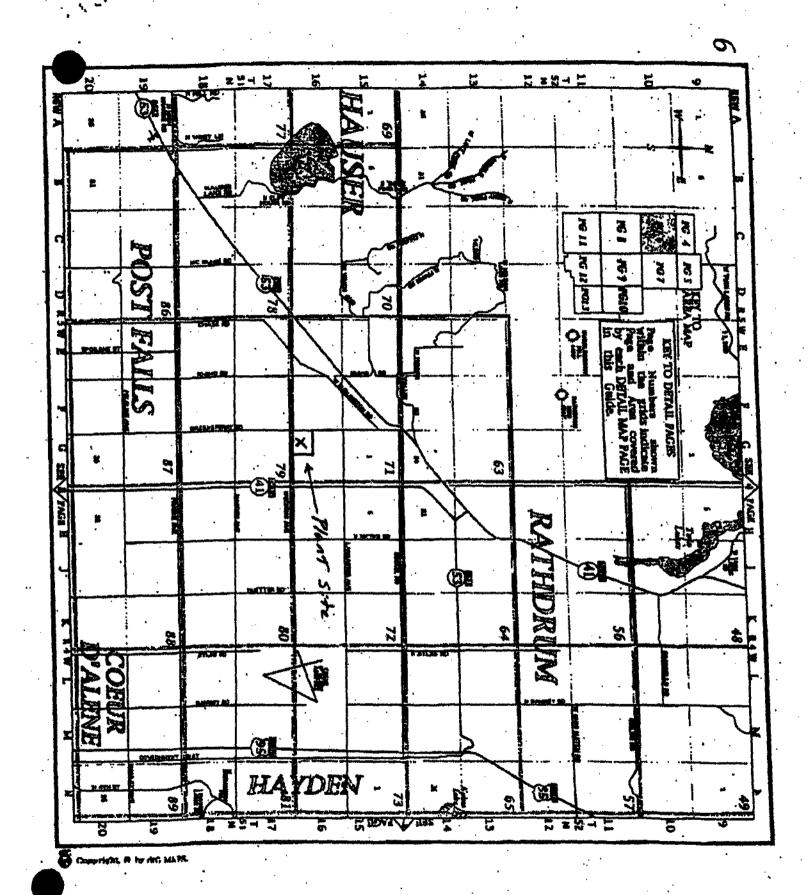


SECTION 3: PROCESS AND MANUFACTURING EQUIPMENT (complete a separate page for each distinct process or manufacturing operation)

APPLICANT SPETEROCENIA	Not applicable to t	his modif. 2. PROC	EBS OR OPERATION IN	.			
MAXIMUM RATED INFUT CAPACITY	4. NORMAL MAXIMUM FEED IN tons/hour	tons/year	8. HOPMAL MAXIMUM torse/hour	PRODUCT OUTPUT tons/year	•		
(tons/hour)*			1,				
PROCESS ECUPMENT		10. POLLUTION CONTROL EQUIPM	NT .	•	-		
		1	Primary	Secondary	÷,		
Type		Туре			-		
· , · · · · · · · · · · · · · · · · · ·		Manufacturer			-		
		Model Number	{				
	-	% Efficiency		<u> </u>	·····		
OPERATING BOMBLE		MANUFACTURER QUARANTEED	Yes r	10			
Childring practure	•	(include guerantee)		•			
Hours per day		For wet scrubber	::				
		water flow		gpm	•		
Weeks per year		pressure drop	#**************************************	ter			
AAAAN bar yaar							
STACK OR EXHAUST DATA		For beghouses:		•			
•	•	sir/cloth ratio		·····			
Stack ID_	· ·	pressure drop		inches of w	eter (
Height_	R		<u>-</u>				
Exit diameter	t	11, CRITERIA POLLUTANT ESTIMATED EMISSIONS					
Exit gas volume_	ecim			-			
Exit gas temperature	,	perficulates		<u>IP/J.k.</u>	tonslyr		
		sulfur dioxide		lb/hr	- tonslyr		
(include a separate page	for each stack if multiple	carbon monoxide		ib/hr	tonelyr		
stacks or vents are used	<i>)</i>	nitrogen oxides		E /hr	tonelyr		
,		voietile organic		· Ib/hr	tonslyr		
•	•	compounds	e calculations and		:		
L TORC AR POLLUTANT ENTM	ATE) BARKAR	I INCADOR	F CONCLARED OF RE BETTE	essuripuciis;			
(include calculations an	; assumptions)	•					
Polluterit		d Emissions	C	ontrolled Emissi	ons		
,	b/vr	tonsýr	<u>ib/m</u>		tone/yr		
	Th/tr	tons/yr	lb/hr	'	tonelyr		
	p/hr	tons/yr	b/l¥	. :-	tone/yr		
	lb/hr	tons/yr	lb/hr		tone/yr		
	lb/ix	tons/yr	· ib/tv		lonsiye		
	b/x	tons/yr	lb/hr	lone/yr			
	lb/hr `	tons/yr	lb/hr	-: -	tonstyr		
	bhr	tons/yr.	lb/hr		tonskyr		
	b/hr .	tons/yr	ib/hr		tonsar		

[&]quot;If units other than tons, please specify.

APPENDIX B FACILITY MAPS



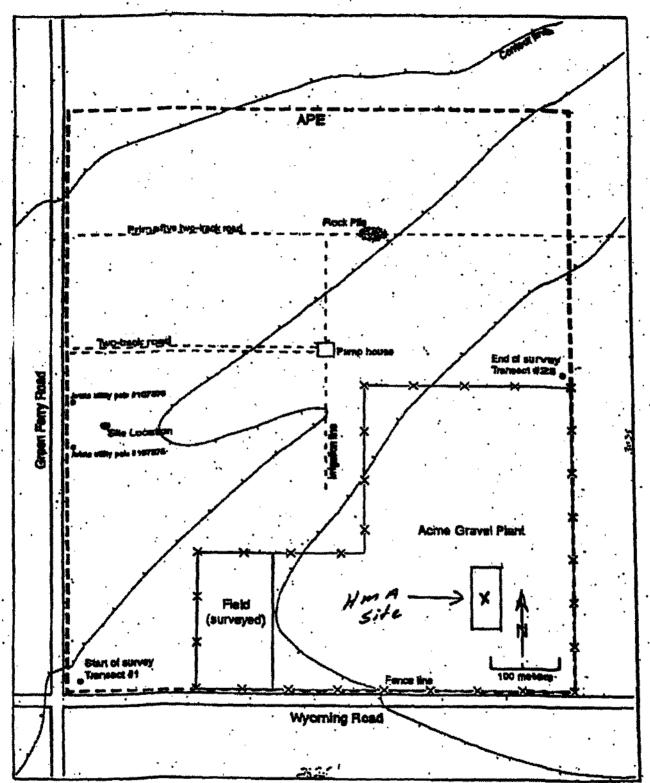


Figure 2. Survey Area. (T.51 N., R.5 W. Sec. 12.)

Northwest Archaeological Associates

APPENDIX C

EMISSION INVENTORY SPREADSHEETS

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Interstate Concrete and Asphalt Company Wyoming Asphalt Plant Couer d'lane, idaho 1/7/2003

Controlled Emissions Summary

Hours of Operation (hrs/yr): Production Rate (Tons/hr HMA):

3,700

400

Total HMA:

1,480,000 Tons per year

Source	PM10 tons/yr	SO2 tons/yr	CO tons/yr	NOx tons/yr	VOC tons/yr
Proposed Dryer	17.02	42.92	96.20	40.70	23.66
Existing Batch Cement	0.80		1		
Existing Rock Crushing Plant Fugitives	59.40	,			• •
Total	77,22	42.92	96.20	40.70	23.68

APPENDIX D

SCREEN3 MODELING OUTPUT FILES

```
*** SCREEN3 MODEL RUN ***
*** VERSION DATED 96043 ***
```

Interstate Concrete and Asphalt - Wyoming Plant

SIMPLE TERRAIN INPUTS: POINT SOURCE TYPE 0.126100 EMISSION RATE (G/S) STACK HEIGHT (M) 9.1440 1.4188 STK INSIDE DIAM (M) STK EXIT VELOCITY (M/S) = 18.8922 408.1500 STK GAS EXIT TEMP (K) = AMBIENT AIR TEMP (K) 293.1500 RECEPTOR HEIGHT (M) 0.0000 URBAN/RURAL OPTION RURAL . BUILDING HEIGHT (M) 0.0000. MIN HORIZ BLDG DIM (M) = 0.0000 .. MAX HORIZ BLDG DIM (M) = 0.0000

THE REGULATORY (DEFAULT) MIXING HEIGHT OPTION WAS SELECTED. THE REGULATORY (DEFAULT) ANEMOMETER HEIGHT OF 10.0 METERS WAS ENTERED.

26.269 N**4/8**3; MOM. FLUX = 129.009 N**4/8**2 BUOY. FLUX =

*** FULL METEOROLOGY ***

*** SCREEN AUTOMATED DISTANCES ***

0. M ABOVE STACK BASE USED FOR FOLLOWING DISTANCES *** *** TERRAIN HEIGHT OF

DIST	CONC	STAB	U10M (M/8)	USTK (M/S)	MIX HT (M)	PLUME HT (M)	SIGNA	EIGNA	
(M)	(UG/M++3)	OLAD	\m/e;	(M/O)	\m/	WT (W)	Y (M)	Z (M)	DWASH
1.	0.000	. 1	1.0	1.0	320.0	257.74	3.95	3.93	NO
100.	0.4232E-01	6	1.0	1.0	10000.0	82.46	21.34	21.08	NO
200.	1.102	4	20.0	20.0	6400.0	20.00	15.74	8.81	390
300.	1.950	4	20.0	20.0	6400.0	20.00	22.81	12.47	MO
400.	1.913	4	20.0	20.0	6400.0	20.00	29.67	1.5.68	. 190
500.	1.667	4	20.0	20.0	6400.0	20.00	36.32	18.64	390
600.	1.476	4	15.0	15.0	4800.0	25.03	42.98	21.73	MO
700.	1.311	1.4	15.0	15.0	4800.0	25.03	49.42	24.50	NO
800.	1.218	4.7	10.0	10.0	3200.0	34.00	56.03	27.71	NO.
900.	1.133	4	10.0	10.0	3200.0	34.00	62.29	30.31	NO
1000.	1.058	4 .	8.0	8.0	2560.0	40.22	68.70	33.30	MO
1100.	0.9921	4	8.0	8.0	2560.0	40.22	74.84	35.26	NO
1200.	0.9288	4	8.0	8.0	2560.0	40.22	80.93	37.17	NO.
1300.	0.8692	4	8.0	8.0	2560.0	40.22	86.97	39.02	190
1400.	0.8136	4	8.0	8.0	2560.0	40.22	92.98	- 40.84	NO.
1500.	0.7623	4	8.0	8.0	2560.0	40.22	98.94	42.60	NO
1600.	0.7267	4	5.0	5.0	1600.0	58.86	105.45	45.70	NO
1700.	0.7033	4	. 5.0	.5.0	1600.0	58.86	111.32	47.35	NO
1800.	0.6794	4	5.0	5.0	1600.0	58.86	117.15	48.97	NO
1900.	0.6557	4	5.0	5.0	1600.0	58.86	122.95	50.56	NO
2000.	0.6690	5	1.5	1.5	10000.0	86.34	98.21		
2100.	0.6876	5	1.5	1.5	10000.0	86.34	102.43	40.89	
2200.	0.7042	-5	1.5		10000.0	86.34	106.64	41.68	
2300.	0.7188	5	1.5		10000.0	86.34	110.84	42.45	•
2400.	0.7327	5	1.0	1.0	10000.0	97.51	115.68	44.93	
2500.	0.7499	5	1.0		10000.0	97.51	119.83	45.66	
2600.	0.7656	5	1.0		10000.0	97.51	123.97	46.38	
2700.	0.7799	5	1.0		10000.0	97.51	128.10	47.09	
2800.	0.7928	5	1.0	1.0		97.51	132.22	47.80	
#111.	* ***	=	7 0		170000 0	97 E1	176 72	AR 50	

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                                   1.0 10000.0
                                                 97.51 140.42
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       0.8147
                                                                49.19
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                      5
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                                   1.0 10000.0
                                                 97.51 160.75
                                                                52.57
                                                                          100
                       5
                            1.0
                                   1.0 10000.0
                                                 97.51 180.83
                                                                55.81
  000.
        0.8641
                                                                          HO
                       5
                            1.0
                                   1.0 10000.0
                                                 97.51 200.68
 4500.
                                                                58.54
        0.8534
                                                                          NO
                       5
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                                   1.0 10000.0
                                                 97.51 220.31
 5000.
        0.8357
                                                                 61.16
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                       6
                             1.0
                                   1.0 10000.0
                                                 82.48 160.07
 5500.
        0.8352
                                                                41.44
                                                                          NO
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                                                 82.48 172.85
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 6000.
        0.8433
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                                                 82.48 185.53
 6500.
        0.8467
                                                                 43.96
                                                                          NO
                       6
                             1.0
                                                 82.48 198.10
        0.8464
                                   1.0 10000.0
                                                                 45.16
 7000.
                                                                          NO
                       6
                             1.0
                                   1.0 10000.0
                                                 82.48 210.58
  7500.
        0.8380
                                                                 46.19
                                                                          NO
        0.8282
                                   1.0 10000.0
                       6
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                                                 82.48 222.97
                                                                 47.19
  8000.
                                                                          NO
                                   1.0 10000.0
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                       б
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        0.8173
                                                                 48.16
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 9000. 0.8056
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                                                 82.48 247.50
                                                                 49.09
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                       6
 9500: 0.7934
                             1.0
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                                                 82.48 259.64
                                                                 50.01
                                                                          NO
                       6
10000. 0.7808
                             1.0
                                   1.0 10000.0
                                                 82.48 271.71
                                                                 50.90
                                                                          NO
                       6
 15000. 0.6556
                             1.0
                                   1.0 10000.0
                                                 82.48 388.99
                                                                 58.75
                                                                          NO
                       6
                             1.0
                                   1.0 10000.0
                                                 82.48 501.39
20000. 0.5443
                                                                 63.83
                                                                          NO
                       6
                             1.0
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                                                 82.48 610.11
25000. 0.4642
                                                                 68.16
                                                                           NO
                       6
                             1.0
30000. 0.4040
                                   1.0 10000.0
                                                 82.48 .715.89
                                                                 71.95
                                                                           NO
                       6
 40000. 0.3193
                             1.0
                                  1.0 10000.0
                                                 82.48 920.46
                                                                  77.38
                                                                           NO.
                       6
                             1.0
                                   1.0 10000.0
                                                 82.48 1117.62
50000. 0.2641
                                                                  81.92
                                                                           NO
MAXIMUM 1-HR CONCENTRATION AT OR BEYOND
                                           1. M:
         1.988
                           20.0 20.0 6400.0 20.00
                                                         25.38
                                                                  13.69
```

DWASH- MEANS NO CALC MADE (CONC = 0.0)

DWASH-NO MEANS NO BUILDING DOWNWASH USED

DWASH-HS MEANS HUBER-SNYDER DOWNWASH USED

DWASH-NA MEANS DOWNWASH NOT APPLICABLE, X<3*LB

*** SUMMARY OF SCREEN MODEL RESULTS ***

CALCULATION	MAX CONC	DIST TO	TERRAIN
PROCEDURE	(UG/M**3)	MAX (M)	HT (M)
	*****	, ,	
OTMOTER TRUBBLIN	1.988	336.	•

APPENDIX E

REFINED MODELING OUTPUT FILES

*** ISCST3 - VERSION 02035 *** *** Interstate Concrete and Asphalt - Wyoming Plant *** Model Executed on 01/15/04 at 11:24:10 *** Input File - F:\2003\ICA03117\Model\ICAWyomingPlant_90_HCHO.DTA Output File - F:\2003\ICA03\17\Model\ICAWyomingFlant 90 HCRO.LST Met File - F:\2003\ICA03117\MetData\Spokane_90.ASC Number of sources -Number of source groups -Number of receptors -4259 *** POINT SOURCE DATA *** NUMBER EMISSION RATE BASE RATE SOURCE (GRAMS/SEC) KLEV.

9.14 . . 408.15 0.66023E-01 507037.0 5291110.0 DRYER

. *** SOURCE IDS DEFINING SOURCE GROUPS ***

(METERS) (METERS) (METERS) (DEG.K)

HRIGHT

KXIT VEL. DIAMETER

(M/SEC)

SOURCE ID: GROUP ID

ALL DRYER

CATS.

VARY .

*** THE SUMMARY OF MAXIMUM ANNUAL (1 YRS) RESULTS ***

** CONC OF HCHO

IN MICROGRAMS/M**3

											. •			NETWORK
GROUP	ID				AVERAGE CONC			REG	CEPTOR	(XR,)	r, zelev, zpla	g) of	TYPE	GRID-ID
-	•			•									"	
ALL	18T	HIGHEST	VALUE	IS	0.03366	AT	(507371.00,	529165	54.00.	684.00,	0.00)	DC	na .
•	2ND	HIGHEST	VALUE	IS	0.03320	λT	(507471.00,		-	684.00.	0.00)	DC	NA .
	3RD	HIGHEST	VALUE	IS	0.03265	AT	(507471.00,	529185	54.00,	683.09,	0.00)	DC	NA .
	4TH	HIGHEST	AYTUR	IS	0.03189	AT	(507571.00,	529195	4.00,	683.61,	0.00)	DC	NA
	5TH	Highest	VALUE	T8	0.03189	AT	(507571.00,	529195	4.00,	683.61,	0.00)	DC	NA
	6TH	HIGHEST	VALUE	IS	0.03189	AT	ŧ	507571.00,	529195	4.00,	683.61,	0.00)	DC	NA
	7 TH	HIGHEST	VALUE	IS	0.03137	AT	(507371.00,	529175	4.00,	683.09,	0.00)	DC	NA
	8TH	HIGHEST	VALUE	I8	0.03092	AT	(507571.00,	529185	4.00,	684.00,	0.00)	DC	NA
	9TH	HIGHEST	VALUE	IS	0.03036	AT	(507471.00,	529195	4.00,	682.90,	0.00)	DC .	NA
	10TH	Highest	VALUE	IS	0.02924	AТ	(507321.00,	529170	4.00,	683.09,	0.00)	DC	NA



parlei derlei ARD. Route to: -Marelini - Coth SF

RECEIVED

MAR - 1 2004

State Air Program

February 27, 2004

Harbi Elshafei
Idaho Dept. of Environmental Quality
1410 N. Hilton
Boise, ID 83706

Subject: Permit to Construct 55-00048 Modification, Rathdrum, Idaho

Dear Mr. Elshafei,

This letter is in response to our telephone conference this AM and I hope that it will clarify our intent.

- 1. RAP Lump Breaker: This is a cold feed bin that sits adjacent to the other aggregate cold feed bins at the plant. The only difference being it feeds a machine that is called a RAP Breaker that basically forces the RAP down through counter rotating drums that break up any oversize pieces prior to being dropped onto the main conveyor which feeds the plant drum. There are RAP crushers available however we have opted not to use one. I have enclosed copies of specifications for a RAP Breaker.
- 2. Concrete Batch Plant: You spoke of a proposed limitation of 5000 hours in the Permit Modification request. I cannot find any wording in the request that would reflect that. On page 2 paragraph 5 of the request it states that we are not requesting a change of limitations for the concrete batch plant.
- Existing Crusher: The crusher that is listed in the currant permit has been somewhat cannibalized and no longer exists for all intensive purposes. All remaining parts will be removed. The only crushing that would take place would be done by a portable crusher as needed.

4. The reason we are requesting a permit that would include an asphalt plant, concrete plant and crusher is that the permit would mirror the existing permit with newer equipment plus allow us to use a portable crusher as needed and not have a crusher sitting on site when not being in use. It is also understood that the crusher would be permitted in the State of Idaho and would not be using a generator for power at this site.

I will be sending you a flow diagram within a few days. Please contact me at 765-1144 if you need additional information to make the requested revision to our permit.

Sincerely,

Corky Witherwax Aggregate Sales/

Environmental Manager

Encl: 2



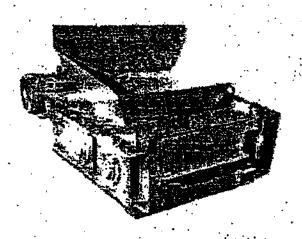
Home About PMI Employment Contacts

Products
Services
Markets
Manufacturers
Inventory
Parts Order Form

Asphalt Recycle -Breakers, Crushers & Systems

RAP Breaker
Rap Systems
RAP Charles
Recycle Systems
Parts

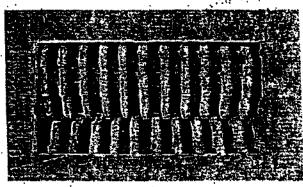
PMI RAP Breaker





Process Machinery, has menutactured this time proven quality roll style breaker for over 20 years.

Now you can buy direct!



Our hardened steel teeth mounted on counter-rotating drums will size RAP to plant requirements.

Ran Breaker Specifications:

- 25 hp direct coupled crosper duty motor
- Double reduction concentric shaft reducer with end-shelf type motor mount
- Hardened steel wear lips on drum teeth
- Extra large receiving hopper to accommodate up to a 36" wide conveyor
- Externally mounted heavy duty plicted flange bearings on drums

- . Externally mounted drive tensioner
- Heavy duty abrasion resistent bott in side wear liners
- Spring return floating drum for tramp iron reject
- ... Lubrication manifold is centrally located for same of maintenance
- Production capacity of up to 150 TPH

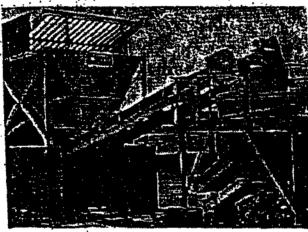


Optional Features:

- Stationary drum cleaner assembly
- Tramp iron and oversize stone reject orizzly assembly
- Electromagnetic tramp iron removal assembly
- · Free standing mounting platform to cover feed churte

Back to Too

RAP Breaker & Recycle Systems



Feed meterial can contain up to "tootball" size congliomerated millings.

Adjustable Grizzly reject tramp iron and oversize material.

The breaker reduces millings to 1" or armalier.

The breaker has training iron protection built in.

Reduced RAP is conveyed to plant.

PMI Recycle Systems

- . Custom Designed to fit your needs
- Stationary and portable designs are available
- Conveyors
- Screens
- Rap bins
- Grizzly landers
- Horizontal shaft impact crushers
- · Rep breakers
- Chutes
- Hoppers
 - Whatever you need to create the system you want!
 - PMI can provide lumkey solutions

Back to Too

APPENDIX B

AIRS Information

P-040101

AIRS/AFS* FACILITY-WIDE CLASSIFICATIOND DATA ENTRY FORM

Facility Name:

Interstate Concrete and Asphalt Company

Facility Location:
AIRS Number:

Rathdrum 055-00048

300	and the second					
SO;	В					Ŭ
NO,	В					U
co	SM			Y	SM80	U
PM ₁₀	В					U
PT (Particulate)	В					U
voc	В			:		U
THAP (Total HAPs)	В				·	A
		APR				
		Ī				

^{*} Aerometric Information Retrieval System (AIRS) Facility Subsystem (AFS)

AIRS/AFS Classification Codes:

- A = Actual or potential emissions of a pollutant are above the applicable major source threshold. For HAPs only, class "A" is applied to each pollutant which is at or above the 10 T/yr threshold, or each pollutant that is below the 10 T/yr threshold, but contributes to a plant total in excess of 25 T/yr of all HAPs.
- SM = Potential emissions fall below applicable major source thresholds if and only if the source complies with federally enforceable regulations or limitations.
- B = Actual and potential emissions below all applicable major source thresholds.
- C ... Class is unknown.
- ND ... Major source thresholds are not defined (e.g., radionuclides).

APPENDIX C

Modeling Analysis

P-040101

MEMORA NDUM

TO:

Harbi Elshafei, Program Office Permit Writer

THROUGH: Mary Anderson, Modeling Coordinator, Program office

FROM:

Dan Pitman, Senior Engineer, Technical Services

DATE:

April 2, 2004

PROJECT NUMBER:

P-040101

SUBJECT:

Modeling Review for Interstate Concrete and Asphalt, Rathdrum, Permit to Construct

Application

Summary

Atmospheric dispersion modeling of facility-wide emissions was submitted in support of a permit to construct application to demonstrate that the stationary source would not cause or significantly contribute to a violation of any ambient air quality standard (IDAPA 58.01.01.203.02). The applicant conducted a full impact analysis on emissions of carbon monoxide, nitrogen dioxide and sulfur dioxide. Emissions of particulate matter were not modeled because emissions of particulate matter decreased as a result of the facility modification. The applicant used the SCREEN3 air dispersion model to determine ambient impacts of carbon monoxide, nitrogen dioxide, sulfur dioxide and 14 toxic air pollutants (TAPs). The applicant's SCREEN3 model results were below standards for all pollutants except formaldehyde. The applicant conducted a refined modeling analysis using the Industrial Source Complex (ISCST3) air dispersion model on emissions of formaldelivde.

numptions used in modeling analysis submitted by the applicant

I MDM 1. 1263 Enaminhetons about ht thoughts with	your securities of the approved
Assumption	Explenation
No Downwash	The applicant simply stated that there was not building influenced downwish.
The facility assumed the asphalt plant would only operate 3,700 hours per year.	Only used in refined modeling analyses for formaldehyde emissions.
Particulate matter emissions are reduced as a result of the facility modification.	Facility is installing a baghouse.

The applicant did not account for downwash in it's air dispersion modeling exercises. DEO conducted sensitivity analyses that accounted for downwash induced by buildings and structures that are adjacent to the stack. The results of DEQ's sensitivity analysis are presented in Section 4 of this memorandum. The submitted modeling analyses in combination with the DEQ Technical Services staff analyses: 1) utilized appropriate methods and models (as clarified by the DEQ staff analyses in Section 4 of the memorandum); 2) was conducted using reasonably accurate or conservative model parameters and input data; 3) adhered to established DEQ guidelines for new source review dispersion modeling; 4) showed that predicted pollutant concentrations from facility-wide emissions. when appropriately combined with background concentrations, were below applicable air quality standards.

2.0 Background information

2.1 Applicable Air Quality Impact Limits

The facility is located in Kootenai County which is designated as unclassifiable for all criteria pollutants. Table 2 summarizes all applicable significant contribution levels, National Ambient Air Quality Standards and acceptable ambient concentrations for all TAPs that are emitted above the TAP screening emission level.

Table 7 Applicable regulatory limits

Pollutant	Averaging Contribution Levels Period (µg/m²)***		Regulatory Limit (µg/m²) ^c	Modeled Value Used		
, , , , , , , , , , , , , , , , , , , ,	8-hour	500	10,000	Highest 2nd highest		
co	l-hour	2000	40,000	Highest 2 nd highest		
	Annual	1	80°	Maximum 1 highest		
SO ₂	24-hour	5	. 365*	Highest 2 ⁶⁶ highest		
· .	3-hour	25	1,300 ^x	Highest 2 ^{ad} highest		
NO ₂	Annual	1	100	Maximum 1 st highest		
2,3,7,8-TCDD	Annual	N/A	2.2E-08	Maximum 1 st highest		
Acetaldehyde	Amnual	NA	0.45	Maximum i highest		
Arsenic	Annual	N/A	2.3E-04	Mexitrrum 1 highest		
Benzene	Annual	NA	0.12	Maximum 1 st highest		
Benzo(a)pyrene	Annual	N/A	3.0E-04	Maximum 1 highest		
Cadmium	Angual	N/A	5.6E-04	Maximum 1 st highest		
Chromium	24-hour	N/A	25	Maximum 1 highest		
Formaldehyde	Annual	NA	7.76-02	Maximum 1 st highest		
HCL.	24-bour	N/A	375	Maximum 1 st highest		
Chromium (VI)	Annuel	N/A 1	8.3E-05	Maximum 1 st highest		
Nickel	Annual	WA .	4.2E-03	Maximum 1" highest		
Phosphorus	24-hour	N/A	5.0	Maximum 1 st highest		
Propionaldehyde	24-hour	N/A	21.5	Maximum i highest		
Quinone	24-hour	·N/A	20.0	Maximum 1st highest		

- a. IDAPA 58.01.01.006.93
- b. Micrograms per cubic meter
- c. IDAPA 58.01.01.577 for criteria pollutants, IDAPA 58.01.01.585 for non-carcinogenic toxic air pollutants. IDAPA 58.01.01.586 for carcinogenic toxic air pollutants.
- d. The maximum 1st highest modeled value is always used for significant impact analysis and for all toxic air pollutants.
- e. Particulate matter with an aerodynamic diameter less than or equal to a nominal ten microsneters
- f. Never expected to be exceeded in any calendar year.
- g. Concentration at any modeled receptor.
- h. Never expected to be exceeded more than once in any calendar year.
- i. Concentration at any modeled receptor when using five years of meteorological data.
- j. The highest 2nd high is considered to be conservative for five years of meteorological data.
- k. Not to be exceeded more than once per year.

2.2 Background Concentrations

Table 3 gives the background concentrations that the State Air Quality Program Office provided for these analyses.

Table 3. Background concentrations.

1 able 5. Dacky Conservation					
Poliutant	Averaging Period	Background concentrations (µm/m²)*			
	i-hour	3,600			
CO	8-hour	2,300			
	3-hour	· · 34			
\$O₂	24-hour	26			
1	Amson				
NO.	Annukl				

a. Micrograms per cubic meter.

3.0 Assessment of Submitted, Certified Modeling Analysis

3.1 Modeling Methodology

Aspen Consulting & Engineering, Inc. performed air dispersion modeling on behalf of Interstate Concrete and Asphalt Company. The applicant performed a full impact assessment for emissions of carbon monoxide, nitrogen dioxide, sulfur dioxide and all TAP emissions that are listed in Table 2. The applicant performed a screening modeling analyses using the SCREEN3 air dispersion model. The applicant's screening modeling analyses results showed that all pollutants except formaldehyde were emitted are rates that caused ambient impacts below applicable standards. A refined modeling analysis was conducted on emissions of formaldehyde using the ISCST3 air dispersion model. The applicant's refined model showed that emissions of formaldehyde caused predicted ambient impacts below the acceptable ambient concentration for formaldehyde. Table 4 summarizes the air dispersion model type and modeling parameters used by the applicant.

The applicant did not account for downwash in either their SCREEN3 or ISCST3 modeling exercises. Technical Services conducted a sensitivity analysis that accounted for downwash. Results of Technical Services sensitivity analysis are presented in Section 4 of this memorandum.

Table 4 Modeling parameters.

Parameter				
Modeling protocol	The applicant did not submit a modeling protocol.	NA NA		
Model Selection	SCREEN3 - Version 96043 ISCST3 - Version 02035	These are appropriate versions.		
Meteorological Data	ISCST3 - Spokane surface and upper air data.	These data sets are the most appropriate data available for use.		
Model Options	ISCST3 Regulatory Defaults were used.	Regulatory defaults are appropriate.		
Land Use	Rural	Rural land me is appropriate.		
Complex Terrain	SCREEN3 - Assumed flat terrain ISCST3 - Considered Complex terrain both simple and complex	surrounding the facility is essentially flat based on re		
Building Downwash	Building Downwash was not considered.	Building downwash should have been included in the modeling exercises. DEQ's sensitivity analyses includes building downwash. See Section 4 of this memorandum.		
Receptor Network	SCREEN3 – iterated to find maximum at or beyond fenceline. ISCST3 – 50 meters along fenceline, 100 meters out to 1 km, 250 meters out to 5 km, and 500 meters out to 10 km.	The receptor placement met the air quality modeling guidelines and was sufficient.		
Facility Layout N/A		The facility layout was verified by scaled plot plans submitted by the applicant on 1/26/04 and 3/22/04.		

3.2 Emission Rates

Table 5 gives the pollutants, emissions rates and hours of operation that were submitted in the permit application and used in the screening modeling analyses.

Table 5. Emissions Rates

Pollutant	Emission Rate (lb/hr)	Hours per Day	Hours per Year
NO.	22	24	8760
co	52	24	8760
so,	23.2	24	8760
2,3,7,8 - TCDD	1.23E-9	24	8760
A cetaldehyde	0,52	24	8760
Arsenic	.0002	24	8760
Benzene	0.156	24	8760
Benzo(a)pyrene	0.0002	24	8760
Cadmium	0.0002	24	8760
Chromium	0.0022	24	8760
Formaldehyde	1.24	7.4	8760
HCI	0.084	24	8760
Chromium VI	0.0002	24	8760
Nickel	0.0252	24	8760
Phosphorus	0.0112	24	8760
Propional dehyde	0.0320	24	8760
Quinone	0.064	24	8760

3.3 Emission Release Parameters

Table 6 gives the stack parameters for the asphalt plant dryer that is the only point source of emissions that was required to be modeled.

Table 6. Stack Parameters

Point Source Dryer				
UTM Easting	507,037 meters			
UTM Northing	5,291,110 meters			
Source Elevation*	683.1 meters			
Height	9.14 meters			
Exit Diameter	1.42 meters			
Exit Gas Volume	29.9 cubic meters per second			
Exit Gas Velocity .	18.9 meters per second			
Exit Oas Temperature	408.2 Kelvin			

3.4 Results

These sections present the results based on the information submitted as certified by the applicant.

3.4.1 Applicant's Screening Analyses Results

The applicant conducted a screening model exercise on emissions of carbon monoxide, sulfur dioxide, nitrogen dioxide and the 14 TAPs listed in Table 5. The applicant stated that an emission rate of one pound per hour was modeled in SCREEN3 and a dispersion factor was developed. The screening dispersion factor determined by the applicant, and verified by DEQ, is 1.988 micrograms per cubic meter (one-hour concentration) per pound per hour of emissions. The applicant stated that

the actual pollutant emission rate was then multiplied by this dispersion factor and them by the appropriate persistence factor to determine the predicted ambient concentration for each relevant averaging period. Table 7 gives the results of the applicant's screening analyses that eare presented in the certified application. Note that the only values in the Table 7 that match what the applicant stated are the annual modeled concentrations for sulfur dioxide and nitrogen dioxide. It is uncertain what the applicant's methodology was to obtain all the other modeled concentrations presented in Table 7. According to the applicant's submittal the only pollutant that exceeded an applicable standard was formaldehyde. The applicant conducted a refined air dispersion modeling analysis or a emissions of formaldehyde.

Table 7 Summary of the Applicant's Screening Model Results

Poliutant	Emission Rate (lb/hr)"	Dispersion Factor (µg/m²/lb/hr)b	Factor France		Modeled Concentration (µg/m²)*	
		1 060	1) -hour	122	
Carbon Monoxide	52.0	1.988	0,7	8-hour	86	
		1.988	0.9	3-hour	49	
Sulfar Dioxide	23.2		0.4	24-hour	22	
Odite Diouss			0.08	Annual	4	
Nitrogen Dioxide	22.0	1.988	0.08	Annual	4	
2.3,7,8-TCDD	1.23E-9	1.988	0.125	Annual	3.79E-19	
Acetaldehyde	0.52	1.988	0.125	Annud	6.72E-02	
Arsenic	0.0002	1.988	0.125	Annual	2.1E-04	
Benzene	0.156	1.988	0.125	Annual	6.05E-03	
Benzo(a)pyrene	0.0002	1.988	0.125	Annual	2.1E-04	
Cadmium	0.0002	1.988	0.125	Annual	1.5E-04	
Chromium	0.0022	1.98	0.4	24-hour	2.1E-3	
Formaldehyde	1.24	1.988	0.125	Annuai	0.382	
HCI	0.084	1.988	0.4	24-hour	0.079	
Chromium VI	0.0002	1.988	0.125	Annual	1.7E-04	
Nickel	0.0252	1.988	0.125	Annual	2.37E-02	
Phosphorus	0.0112	1.988	0.4	24-hour	1.06E-02	
Propionaldehyde	0.0520	1.988	0.4	24-hour	4.89E-02	
Ovinone	0.064	1.988	0.4	24-hour	6.03E-02	

a. Pound per hour

b. Micrograms per cubic meter per pound per hour

c. Micrograms per cubic meter

Table 8. Applicant's criteria pollutant ambient impact analysis results

Pollutant	Averaging Period	Facility Ambient Impact (µg/m³)*	Background Concentration (µg/m ³)*	Total Ambient concentration (µg/m²) ¹	NAAQS ^b	Percent of NAAQS ^b
CO 8-hour	1-hour	122	3,600	3,722	40,000	9.3
	8-hour	86	2,300	2,386	10,000	23.9
SO ₂ 24-b	3-hour	49	34	83	1,300	6.4
	24-hour	22	26	48	365	13.1
	Annuel	4	8	12	80	15
NO ₂	Annua	4	17	21	100	21

Micrograms per cubic meter

b. National Ambient Air Quality Standards

3.4.2 Applicant's Refined Modeling Analyses Results.

The applicant conducted a refined modeling analysis on emissions of formaldehyde using the ISCST3 air dispersion model. Table 9 presents the applicant's certified results for the refined modeling of formaldehyde emissions. The applicant's refined modeling analysis included limiting the asphalt dryer annual hours of operation to 3,700 hours per year. The applicant did not account for building and structure downwash in it's refined modeling analysis. All other aspects of the refined modeling analysis met DEQ modeling guidelines.

Table 9. Applicant's Formaldehyde Refined Modeling Analysis Results

Model Year	Modeled Emission Rate (lb/kr)*	Modeled Annual Concentration (µg/m²)	idaho AACC (μg/m³) ^h
1987		0.0252	
1988		0.0316	
1989	-0.524	0.0261	0.077
1990		0.0337	•
1991		0.0238	

- a. Pound per hour
- b. Micrograms per cubic meter

4.0 DEQ Sensitivity Analysis Results

The applicant did not account for building and structure downwash in air dispersion modeling. Technical Services conducted sensitivity analyses using the same ISCST3 input parameters that the applicant used except that Technical Services included all buildings and structures that are adjacent to the stack. The applicant provided the dimensions of all buildings and structures that surround the stack in an application supplement received by DEQ on March 22, 2004. Since there is only one point source of emissions that must be modeled an emission rate of one pound per hour was modeled for use in developing dispersion factors. Dispersion factors were determined for each averaging period in micrograms per cubic meter per pound per hour. Actual emissions of carbon monoxide, sulfur dioxide, nitrogen dioxide and the 14 TAPs listed in Table 5 were then multiplied times the appropriate dispersion factor to obtain the predicted ambient concentrations for each pollutant. All annual concentrations in Technical Services sensitivity analysis were determined based on 3,700 hours per year of operation. All 24-hour and shorter averaging periods are based on 24 hours per day of operation.

The results of Technical Services sensitivity analyses are presented in Table 10, as is a comparison to the applicant's dispersion modeling results. The differences between Technical Services modeled impacts and the applicant's modeled impacts are in part due to the fact that the applicant did not account for operating only 3,700 hours per year, except for in the case of formaldehyde, and the applicant did not include downwash.

Pollutant	Emission Rate (lb/hr) ^a	Dispersion Factor (µg/m³/lb/hr)³	Averaging Period	Technical Servicing Modeled Concentration (µg/m³)*	Applicant's Certifiel Modelled Concentrations (µg/m²)*
	60.0	6.72	1-hour	349.4	122
Carbon Monoxide	52.0	2.02	8-hour	105.0	\$6
		3.25	3-hour	75.4	49
Sulfur Dioxide	23.2	0.8	24-hour	18.6	22
Out Dionite		0.077	Anoual*	0.75	4
Nitrogen Dioxide	22.0	0.077	Ansoval*	0.72	4
2,3,7,8-TCDD	1.23E-9	0.077	Annual	4.0E-11	3.79E-19
Acetaldehyde	0.52	0.077	Annual*	1.7E-2	6.72E-2
Arsenic	0.0002	0.077	Amoual	6.5E-6	2.1E-4
Benzene	0.156	0.077	Ammal	5.1 E-3	6.05E-3
Benzo(a)pyrene	0.0002	0.077	Annual*	6.5E-6	2.16-4
Cadmium	9.0002	0.077	Annual*	6.5E-6	1.58-4
Chromium	0.0022	0.9	24-hour	1.98E-3	2.1E-3
Formuldehyde	1.24	0.077	Annual*	4.0E-2	3.37E-2
HCI	0.084	0.9	24-hour*	0.076	0.079
Chromium VI	0.0002	0.077	Annual*	6.5E-6	1.7E-4
Nickel	0.0252	0.077	Anmal*	8.2E-4	2.37E-2
Phosphorus	0.0112	0.9	24-hour	0.010	0.0106
Propionaldehyde	0.0520	0.9	24-hour ^e	0.047	0.049
Quinone	0.064	0.9	24-hour	0.057	0.0603

- Pounds per hour
- b. Micrograms per cubic meter per pound per hour
- c. Micrograms per cubic meter
 d. Highest 2nd highest
 e. Maximum 1nd highest

Tables 11 and 12 compare Technical Services sensitivity modeling results to the applicable standards.

Table 11. Technical Services criteria pollutant ambient impact analysis results

Pollutant	Averaging Period	Facility Ambient Impact (µg/m³)°	Rackground Concentration (µg/m³)*	Total Ambient concentration (µg/m²)*	NAAQS'	Percent of NAAQS ^b
	1-hour	349,4	3,600	3,949.4	40,000	9.9
CO	8-hour	105.0	2,300	2,405.0	10,000	24
	3-hour	75.4	34	109.4	1,300	8.4
SO ₂	24-hour	18.6	26	44,6	365	12.2
Annual	Annual	0.75	8	8.75	80	10.9
NO ₂	Annual	0.72	17	17.72	100	17.7

Micrograms per cubic meter

b. National Ambient Air Quality Standards

Table 12 Technical Services toxic air pollutant ambient impact results

Pollutant	Technical Services Modeled Concentration (µg/m³)*	Toxic Air Pollutant Standard (µg/m³)*	Percent of Toxic Air Pollutant Standard
2,3,7,8-TCDD	4.0E-11	2.2E-8	0.18
Acetaldehyde	1.7E-2	. 0.45	3.8
Arsenic	6.5E-6	2.3E-4	2,8
Benzene	5.1E-3	0.12	4.3
Benzo(a)pyrene	6.5E-6	3.0E-4	2.2
Cadmium	6.5E-6	5.6E-4	1.2
Chromium	1.9 8 E-3	25	\$90.0
Formaldebyde	4.0E-2	0.077	51.9
HCI	0.076	375	0.02
Chromium VI	6,5E-6	8,3E-5	7.8
Nickel	8.2E-4	4.25-3	19.5
Phosphorus	0.01	5	0.2
Propionaldehyde	0.047	21,5	0.21
Quinone	0.057	. 20	0.29

a. Micrograms per cubic meter

APPENDIX D

PTC Processing Fee Calculations
P-040101

PTC Fee Calculation

Instructions:

Fill in the following information and answer the following questions with a Y or N. Enter the emissions increases and decreases for each pollutant in the table.

Company: Interstate Concrete, Rathdrum Address: 845 West Kathleen Avenue

City: Coeur d'Alene

State: ID Zip Code: 83815

Facility Contact: Corky Witherwax

Title: Environmental Manager

AIRS No.: 055-00048

N Does this facility qualify for a general permit (i.e. concrete batch plant, hot-mix asphalt plant)? Y/N

Y Did this permit require engineering analysis? Y/N

N Is this a PSD permit Y/N (IDAPA 58.01.01.205.04)

	=4:.4;		
Total:	227.57	83	144.6
TAPS/HAPS	7.05	0	7.05
VOC	23.68	0	23.68
PM10	17.02	26.5	-9.48
CO	96.20	36.8	59.40
SO ₂	42.92	0	42.92
NO _X SO ₂ CO PM10	40.70	19.7	21.00
Fattage	e kontine milion procession		

Comments:

Permit to construct processing fee, in accordance with IDAPA 58.01.01.225.

APPENDIX E

Response to Public Comments
P-040101

Response to Public Comments Submitted During the Public Comment Period for Interstate Concrete and Asphalt Company, Rathdrum Permit to Construct No. P-040101 Facility ID No. 055-00048

As required by IDAPA 58.01.01.209.01.c of the Rules for the Control of Air Pollution in Idaho (Rules), the Idaho Department of Environmental Quality (DEQ) provided proposed Permit to Construct (PTC) No. P-040101 for Interstate Concrete and Asphalt Company (Interstate) located in Rathdrum, for public notice and comment. Public comment packages, which included the application materials, the proposed permit, and the associated air quality statement of basis, were made available for public review at DEQ's Coeur d'Alene Regional Office, Rathdrum Public Library, and DEQ's state office in Boise. A copy of the proposed PTC No. P-040101 and the statement of basis was also posted on DEQ's Web site. The public comment period for the PTC was provided from June 1 through June 30, 2004.

The following is a summary list of all documents received from the public containing comments on the above referenced permit action.

- 1. Randy Tetzner Letter to DEQ, dated 6-30-04
- Randy Tetzner Document to DEO, dated 6-30-04

This section provides the air quality related comments submitted on the proposed action and DEQ's responses to those comments. Based on the application materials and the Rules, DEQ has responded only to those comments that directly relate to the air quality aspects of the permit.

1. Comments taken from Randy Tetzner Letter, dated 6-30-04

Comment No. 1

I have found this comment procedure confusing. I was so confused I was unaware of a similar permit request by Interstate to burn waste oil even closer to our home. I would like my comments about their Rathdrum Idaho facility to be added to the Hayden Lake comments, regardless if the comment period is over or not. I emailed Ms. Lechtenberg numerous times concerning start dates for comments and never received answers. As a result I did not know my rights, interstate should not be allowed to pollute and have DEQ mislead citizens about how the comment process works.

DEQ Response to Comment No. 1

A 30-day public comment period was provided from May 20 through June 18, 2004, for the proposed PTC for Interstate Concrete's Hayden Lake facility. A 30-day public comment period was also provided from June 1 through June 30, 2004, for the proposed PTC for Interstate Concrete's Rathdrum facility. Public comments were only received during the Rathdrum comment period. Per commenter request, DEQ considered the comments received for the Rathdrum permit also for the Hayden Lake permit.

In regards to proper public notification procedure, the public was notified of both comment periods through several methods. First, a legal notice for each public comment period was published in the Coeur d' Alene newspaper which provided information about the purpose of the comment period, dates of the public comment period, the address to submit public comments, and the location of materials for review (application, draft permit, and DEQ's analysis). In addition, public notice information was also provided on DEQ's website at www.deq.state.id.us which presents the same information as in the legal notice, and also allows the user to download copies of the draft permit and DEQ's analysis (known as the Statement of Basis) in PDF format. DEQ also maintains an interested parties list which provides email notification of all upcoming public comment periods. In addition to this list, an email notification of a public comment period is also provided to the person or persons who requested a public comment period on a specific permit. DEQ records indicate that the commenter was provided email notification on both comment periods.

2. Comments taken from Randy Tetzner Document, dated 6-30-04

Comment No. 2

"...By allowing this company to burn waste oil, we are already going to be the recipient of hundreds of tons of extra pollutants, and those are the ones the EPA finds in oil that is supposed to be good. Factor in the fact that as many as 16,000 different locations will be needed to get the oil and you have a nightmare of trying to ensure the contaminated oil stays away from 1daho. The actual figure of needed sites will probably go as high as 30,000 because many producers of waste oil only get their oil picked up every 2 to 3 months. Monthly pick-ups are not the norm. Most of the oil comes from business that have pickups every 2 to 3 months. The problem is that all the testing is done before the oil is ever even shipped. Oil can sit for weeks and months after it is tested, it can be further contaminated. Despite the fact that halogenated wastes are not a part of waste oil, contamination of waste oil when it is off site. The only way to ensure the law is followed is to have each and every shipment checked when it is delivered to Interstate. Hopefully the permit will be denied making this point moot. There is no way to track backwards were a contaminant came from. No one tests oil by the tanker load; the oil is tested on the producer's tanks farms, which have storage from 10,000 to 250,000 gallons. After the oil is put in a tanker there is no control over what can happen..."

DEQ Response to Comment No. 2

The permits for both facilities include the following requirements for used oil:

Used Oil Specifications

In accordance with 40 CFR 279.11, with the exception of total halogens which are limited to 1,000 ppm, used oil burned for energy recovery shall not exceed any of the allowable levels of the constituents and property listed in Table 2.3.

TABLE 2.3 USED OIL SPECIFICATIONS

Arsenic	5 ppm² maximum		
Cadmium	2 ppm maximum		
Chromium	10 ppm maximum		
Lead	100 ppm maximum		
Flash point	100 deg. F minimum		
Total halogens	1,000 ppm maximum		

The specification does not apply to mixtures of used oil and hazardous waste that continue to be regulated as hazardous waste (see 40 CFR 279.10(b)).

Used Oil Fuel Certification

The permittee shall demonstrate compliance with the used oil fuel specifications in Permit Condition 2.9 by obtaining a used oil fuel certification from the used oil fuel supplier on an as-received basis. The certification shall include the following information:

- The name and address of the used oil supplier
- The measured concentration, expressed as ppm, of each constituent listed in Table 2.2
- The flash point of the used oil expressed as degrees Fahrenheit
- The analytical method or methods used to determine the concentration of each constituent and property (flash point) listed in Table 2.2
- The date and location of each sample
- The date of each certification analysis

² Parts per million

Records of each certification shall remain on site for the most recent two-year period and shall be made available to DEQ representatives upon request.

This permit condition will ensure that the oil delivered at the site has a certification from the supplier on an as-received basis.

Comment No. 3

In the January 18th report, which was produced by Aspen Consulting & Engineering, Inc. they describe Interstates current set up as one, using natural gas. (Introduction 1.0) and that the new set up will have a "bag house" control. As I understand it the baghouse is to collect large particulate contamination that is only found when burning waste oil. The report continues to state that even though RAP is being swapped for cold aggregate, this would mean no increase in particulate contamination. I find this difficult to follow. Increasing production rates by 100 tons an hour, adding a bag house and burning waste oil will most definitely cause on increase in particulate emissions.

DEQ Response to Comment No. 3

A baghouse is a very effective control device for controlling particulate matter emissions. In most cases, the collection efficiency of a baghouse is greater than 99% for particulate matter. Regardless, the PM standard for this facility is 0.04 grains per dry standard cubic foot. The permittee is required to demonstrate compliance with this standard under worst-case normal operations which are, in this case, using RAP and burning used oil. To ensure the baghouse is operated optimally, the permittee is required to develop an O&M manual based on the baghouse manufacturers design operating specifications.

Comment No. 4

The report by Aspen also shows a drawing of an asphalt plant, presumably the one Interstate has. The drawing however is simply a plagiarized copy of EPA diagrams from their AP-42, Section 11 et seq. publication. The EPA has 3 such drawings, while one can clearly see Aspen used a altered copy, they did not cite the EPA publication as the original creator of the diagram, leading people to think they were looking at a diagram of what exists in Rathdrum at present. The EPA diagrams have either a RAP Bin & Conveyor or a Collector in the upper left of the diagrams. The one submitted as figure one in Aspen's report has neither. Does the Aspen diagram accurately depict what Interstate has in Rathdrum? Does the missing a RAP Bin & Conveyor or a Collector shown on EPA diagrams of asphalt mixing plants but not on Interstates submission mean anything? Is Interstate using new technology not even known to the EPA? Why are those items missing from Interstate's proposal diagram?

DEQ Response to Comment No. 4

The Aspen diagram in your comments was obtained from AP-42. On February 27, 2004, DEQ requested, via telephone, that Interstate submit a process description of the facility to better represent the actual HMA plant. On March 8, 2004, Interstate submitted to DEQ a modification to the flow diagram included in the original PTC application. DEQ used the modified flow diagram of the HMA plant and described it in the PTC process description of PTC No. P-040101. The eight cold feed bins and the conveyor are included in the process description (Section 2.1) of the permit. DEQ, however, included in the public comment package a flow diagram that was included in the original PTC application. For clarification, a copy of the actual plant flow diagram that was sent to DEQ on March 8, 2004 is included in Appendix F of the statement of basis.

Comment No. 5

PM₁₀ is Particulate Matter; the report is 77.2 tons per year. Aspen does not give enough information for me to check the figures they are using to calculate PM₁₀. But in their spreadsheet in Appendix C they use the figure of .032 lb per ton. To arrive at the figure of 77.2 tons I see they added the PM₁₀ from existing batch cement and exiting rock crushing plant fugitives, is this assumption correct? Also how does this new and higher PM₁₀ amount affect our air? What can the particulate carry into the air from interstates site?

DEQ Response to Comment No. 5

Yes, Aspen's assumption is correct. The 77.22 T/yr of PM_{10} emissions was obtained by adding emissions from the following sources at the facility:

Proposed HMA Dryer = 17.02 T/yr

Existing Batch Plant Cement = 0.8 T/yr (Tier II operating permit No.055-00048, issued 11/27/02)
Existing Rock Crushing Plant (Fugitives) = 59.40 T/yr (Tier II operating permit No.055-00048, issued 11/27/02)

The 17.02 T/yr of PM₁₀ emissions from the proposed HMA dryer were calculated by Aspen Engineering, and the emissions calculations were reviewed by Dan Pitman, DEQ's Senior Engineer. Emissions inventory for the criteria air pollutants, TAPs, and HAPs from the HMA dryer are included in Appendix A of DEQ's statement of basis. Here is how the 17.02 T/yr were obtained:

Given:

HMA Production Rate: 400 T/yr

Hours of Operation Limits: 3,700 hrs/yr

PM₁₀ Emission Factor for Drum Mix Asphalt Plant: 0.023 lbs/T (Table 11.1-13, AP-42, Hot Mix Asphalt Plants, 3/04)

1 ton (T) = 2,000 lbs

Therefore, PM₁₀ emissions = (400 T/hr)(3,700 hrs/yr)(0.023 lbs/T)(1 T/2,000 lbs) = 17.02 T/yr

The PM₁₀ emissions from the proposed HMA dryer will be lower than the PM₁₀ emissions from the existing dryer. The PM₁₀ emissions from the existing dryer are 10.4 lbs/hr and 26.5 T/yr, whereas the PM₁₀ emissions from the proposed HMA dryer will be 9.2 lbs/hr and 17.02 T/yr. Therefore, there will be a net decrease in PM₁₀ emissions of 1.2 lb/hr and 9.48 T/yr as a result of replacing the old dryer with the new dryer.

Comment No. 6

In the modeling analysis from interstate that was reviewed, in Section 3.4.1 the reviewer states they are not aware of the methodology utilized by interstate to arrive at the figures they submitted in Table 7. It shows Interstate will also go over the acceptable levels of formaldehyde. If the reviewer is unsure how Interstate arrived at it's figures, how can the citizens of Idaho and my family be convinced the report is not flawed? How can we be sure Interstate has not submitted a proposal that is dangerous or otherwise illegal? There was also a comment from DEQ stating the Applicant's formaldehyde refined Modeling Analysis Results (Table 9 Section 3.4.2 of applicants modeling analysis Appendix C) this model was submitted because of high levels of formaldehyde emissions burning waste oil. This submitted model shows acceptable rates of formaldehyde. I do not understand the 1987 through 1991 data submitted, nor do I understand how the modeling was done. Seeing as how this is the first waste oil burning asphalt plant in N. Idaho these figures were probably developed on some theoretical level, and to my surprise are suddenly acceptable levels. The only way to get actual emission outputs is to burn the waste oil in Interstates Dryer and test the emissions several times over a period of a month or two. This submitted model to me has no basis in fact. The EPA supplies the data as to what is emitted when you burn waste oil in an asphalt plant and now suddenly some mathematician has submitted data, which miraculously lowers the rate of formaldehyde emissions? I think of this model as a sham.

DEO Response to Comment No. 6

Section 3.4.1 of DEQ's modeling analysis technical memorandum states that "it is uncertain what the applicant's methodology was to obtain all other modeled concentrations presented in Table 7." Because of this uncertainty, DEQ performed a modeling sensitivity analysis. The results of the sensitivity analysis are presented in Table 10, Section 4.0 of DEQ's modeling technical memorandum, which compares the applicant's modeling results against DEQ's sensitivity analyses modeled results. All pollutants modeled by DEQ show compliance with National Ambient Air Quality Standards (NAAQS) and TAPs increments.

Formaldehyde is a TAP. The modeled formaldehyde emissions also showed compliance with the Acceptable Ambient Concentration for Carcinogens (AACC) value of 7.7E-02 ug/m³. The modeled value is 4.0E-02 ug/m³, which is less than the AACC value.

The facility is required to demonstrate compliance with NAAQS and the Acceptable Ambient Concentration for Carcinogens (AACC) and Non-Carcinogens (AAC). This demonstration is accomplished by using models and procedures required by the "Guideline on Air Quality Model" (40 CFR Part 51, Appendix W). The "1987 through 1991" refers to the years of meteorological data used in the model to estimate the ambient concentrations resulting from the proposed project. The "Guideline on Air Quality Models" (40 CFR 51, Appendix W) states: "the modeler user should acquire enough meteorological data to ensure that worst-case meteorological conditions are adequately represented in the model results."

Interstate Concrete used meteorological data from the National Weather Service station located at the Spokane Airport. Data was used for the years 1987 through 1991 because DEQ determined these years represent the most recent occurrence of worst-case weather conditions for air quality, meeting the requirement set in the "Guideline on Air Quality Models."

Comment No. 7

I do see from the information provided that Interstate is increasing the amount of pollutants in the air an additional 20 tons of NOR, an additional 43 tons of Sulfur Dioxide, it appears that by burning natural gas they did not produce this previously. One of the down sides of burning waste oil is the incredible amounts of sulfur dioxide produced, .055 lbs per ton. An additional 60 tons of Carbon Monoxide awaits each of us along with 24 tons of VOC's and eight tons of TAPS/HAPS. The report states we get 10 tons less of PM₁₀ per year, I do not see how a reduction can be made using waste oil as the fuel. I see Interstate pays a \$7,500.00 permit fee, is this annual or one time? Either way it is a cheap way to pollute the air.

DEQ Response to Comment No. 7

The increase of emissions for NO_x, SO₂, CO, and TAPs increments, when modeled, showed compliance with NAAOs—refer to Appendix A of DEO's statement of basis.

Please refer to Response to Comment No. 5 to see the annual reduction in PM₁₀ emissions rates calculations resulted from replacing the old dryer with the new one.

With regard to the \$7,500.00 permit fee, it is a one time processing fee that the company paid in accordance with IDAPA 58.01.01.225. In accordance with IDAPA 58.01.01.225, the fee for a non-major new source or modification to existing source with increase of emissions of 100 tons per year shall be \$7,500.00.

Comment No. 8

I was only able to find the following break down of how to calculate costs per ton to produce asphalt I have asked interstate how much natural gas is used and the cost of the natural gas to produce one ton of asphalt. These telephone calls go unreturned. Surprisingly the environmental manger, Corky Witherwax has no clue as to how much in natural gas does it cost to produce a ton of asphalt, nor was the company willing to tell me any cost savings they would realize by using waste oil. From the below information it seems one high cost is Salaries and Benefits using up 30% of the incoming cash flow. Interstate also has to support the people who do nothing but produce and deliver concrete. If it shows that there cost savings burning waste oil are minimal, why allow it? Burning waste oil emits a lot of contaminants into the air and is a breeding ground for unknown contaminants not even routinely tested for. I have a feeling the cost savings will be significant for the company to invest in this ability to burn waste oil. Therefore I believe the company will have the resources to test each and every load of waste oil once it arrives at its proposed Rathdrum site and before it is burned. There also needs to be included in the permit a contingency plan of what to do and who to call if they get a bad load of oil. This new hazardous material will also require upgrades with the current fire protection agencies Haz-Mat team. How much money will interstate be paying for this additional burden? Or perhaps I will have to pay it as an increase in my property taxes? I do not think that would be fair for the taxpayers to boot additional funding required keeping us safe. Eventually there will be a spill and Haz-Mat will have to respond, so who pays for their start up costs?

DEQ Response to Comment No. 8

The air quality permit addresses the requirements of IDAPA 58.01.01.200-228 for issuing permits to construct. With regard to used oil, the permit contains limits to assure associated air pollutant emissions do not exceed applicable standards. The permit requires that the used oil be certified on an as-received basis to assure the oil does not contain any contaminants in excess of the imposed limits.

Comment No. 9

Stack emissions need to be taken at least 8 times in the next 2 years to ensure other contaminants are not being introduced and that the alleged amounts deemed to be tolerated are not exceeded. After that require 2 stack emissions tests per year. It is unfair for one test a year at a known time, which would motivate anyone to ensure they burn cleaner.

DEQ Response to Comment No. 9

Performance testing is only required for PM emissions in accordance with 40 CFR 60.92. Limits placed on the concentration of the contaminants in the used oil are shown through modeling to not violate any respective ambient standard. As such, DEQ is not requiring testing of the waste oil contaminants. To assure the facility continues to meet the NSPS grain loading and opacity standards, emissions testing is required on a frequency of no less than once every five years.

Comment No. 10

DEQ should expand the testing for other heavy metals, the federal regulations gives the state the right to make on-spec oil requirements more stringent than federal regulations.

DEQ Response to Comment No. 10

DEQ requires that the facility conduct a PM emissions test. The operating temperature of a hot-mix asphalt plant is far below the melting point of any of the metals identified as contaminants in the used oil. Consequently, the metals should be emitted as particulate, which will be part of that is measured. So long as the facility meets the NSPS grain loading requirement and the used oil contaminants do not exceed the permit limits, compliance with ambient air quality standards will be demonstrated. End.

APPENDIX F

HMA Plant Flow diagram
P-040101

MAR - 8 2004

ECEIVED

CETATURENT OF ENVIRONMENTAL CUALITY

March 5, 2004

Harbi Elshafei Idaho Dept. of Environmental Quality 1410 N. Hilton Boise, ID 83706

Subject: Permit to Construct 55-00048 Modification Flow Chart, Rathdrum, Idaho

Dear Mr. Elshafei,

Enclosed you will find a flow chart for the requested permit modification. As you will see I have used the flow diagram for a counter-flow drum mix plant from AP42 for it does represent the configuration of the new plant. I have added to the diagram four (4) additional cold feed bins to better reflect the actual plant. By adding the cold feed bins, the through put of the plant is not increased. The added bins are to accommodate different sizes of aggregate for different types of asphalt mix.

Please contact me at 765-1144 if you need additional information to make the requested revision to our permit.

Sincerely,

Corky Witherwax Aggregate Sales/

Environmental Manager

Encl: 1

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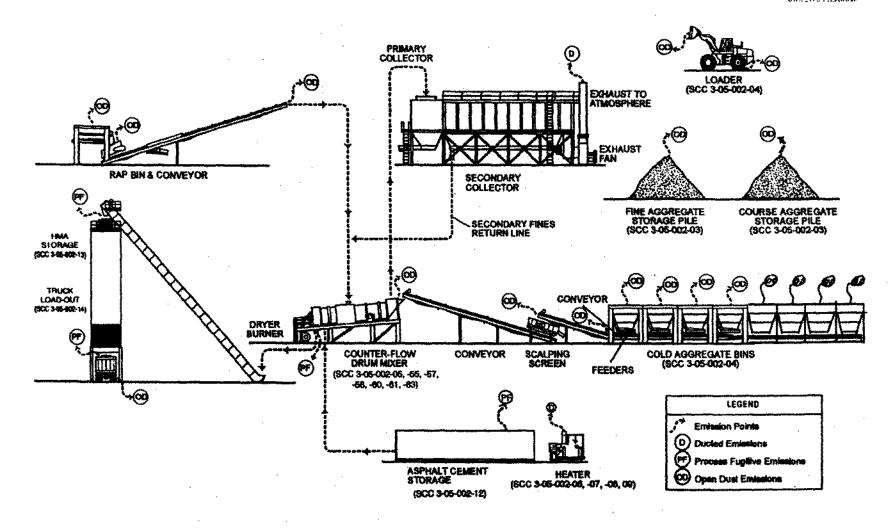
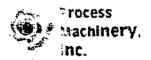


Figure 2-3. General process flow diagram for counter-flow drum mix asphalt plants (source classification codes in parentheses).

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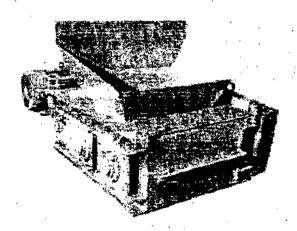
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Asphalt Recycle --

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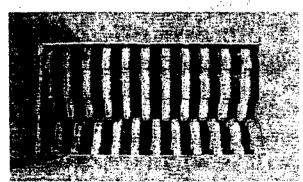
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Process Machinery has manufactured this time proven quality roll style breaker for over 20 years.

Now you c≘n buy direct!



Our hardened steel teeth mounted on counter-rotating drums will size RAP to plant requirements.

Rap Breaker Specifications:

- 25 hp direct coupled crusher duty moto:
- Double reduction concentric shaft reducer with end-shelf type motor mount
- Hardened steel wear lips on drum teeth
- Extra large receiving hopper to accommodate up to a 36" wide conveyor
- Externally mounted heavy duty piloted flange bearings on drums

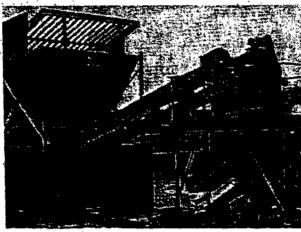
- Externally mounted drive tensioner
- . Heavy duty abrasion resistant bott in side wear liners
- Spring return floating drum for tramp iron reject
- Lubrication manifold is centrally located for ease of maintenance



- Electromagnetic tramp iron removal assembly
- Free standing mounting platform to cover feed chute

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Feed material can contain up to "football" size conglomerated millings.

Adjustable Grizzly reject tramp iron and oversize material.

The breaker reduces millings to 1" or smaller.

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Reduced RAP is conveyed to plant.

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- · Horizontal shaft impact crushers
- Rap breakers
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 - PMI can provide turnkey solutions

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